

## **6. CHARACTERIZATION USING MONTE CARLO N-PARTICLE CALCULATION**

This section describes the MCNP4B (LANL 1997) calculation techniques and tools that are employed to predict accurately the activation product concentrations or radionuclide inventories for an irradiated beryllium block.

### **6.1 Requirements for Characterization Calculations**

Characterization of the beryllium blocks relies on both calculation and measurement techniques, both of which play critical roles in the process and build confidence in the conclusions. The measurements of assay samples taken from the blocks remaining in the ATR storage canal provide valuable information, but typically are small samples taken from a few specific locations around the block and ultimately provide only a limited number of radionuclide concentrations. However, these measurement samples do provide direct characterization information and validate the corresponding calculated radionuclides at these specific locations. These in turn provide some level of validation of the computer codes, computer models, calculation methodology, and the radionuclide inventories calculated for the blocks. The calculated radionuclide inventory is then relied on to provide full characterization information for each whole beryllium block.

The goal was to simulate through calculation the irradiation environment to which the beryllium blocks were exposed during their residency in the ATR core. Sophisticated computer codes, relatively large computer models of the reactors, and substantial input data are required for such simulation. The computer codes, methodology, and input data are discussed below in some detail. The primary strength of the calculation characterization technique is its ability to provide activation product concentrations anywhere in the beryllium block for any radionuclide of interest and at any point in time during or following the irradiation.

This powerful calculation technique provides the capability to estimate an average radionuclide inventory for an entire beryllium block or OSCC, or a local radionuclide inventory of any selected sub-volume of either component. The ability to calculate a local radionuclide inventory allows for direct comparison of radionuclide concentrations taken from small assay samples. Comparisons of calculated versus measured radionuclide concentrations provide confidence in the total calculated radionuclide inventory, and the total calculated radionuclide inventory is relied on heavily for the average beryllium block characterization.

Samples taken at Sites 1 and 2 on the 010R beryllium block (see Figure 6-1) showed large differences in TRU concentrations. The differences were attributed to the large variations in neutron flux and neutron energy spectra between the two sample locations. Clearly, at some point between the front face of the beryllium block (Site 2) and the peripheral edge of the block top surface (Site 1), the TRU concentration reached a maximum because the calculated average block TRU concentration was higher than at either Site 1 or Site 2. This conclusion led to developing a segmented beryllium block model as part of the calculation characterization effort to establish a three-dimensional TRU distribution within the 010R beryllium block. The results of the modeling are discussed below, and help identify those regions of maximum TRU concentration in the blocks.

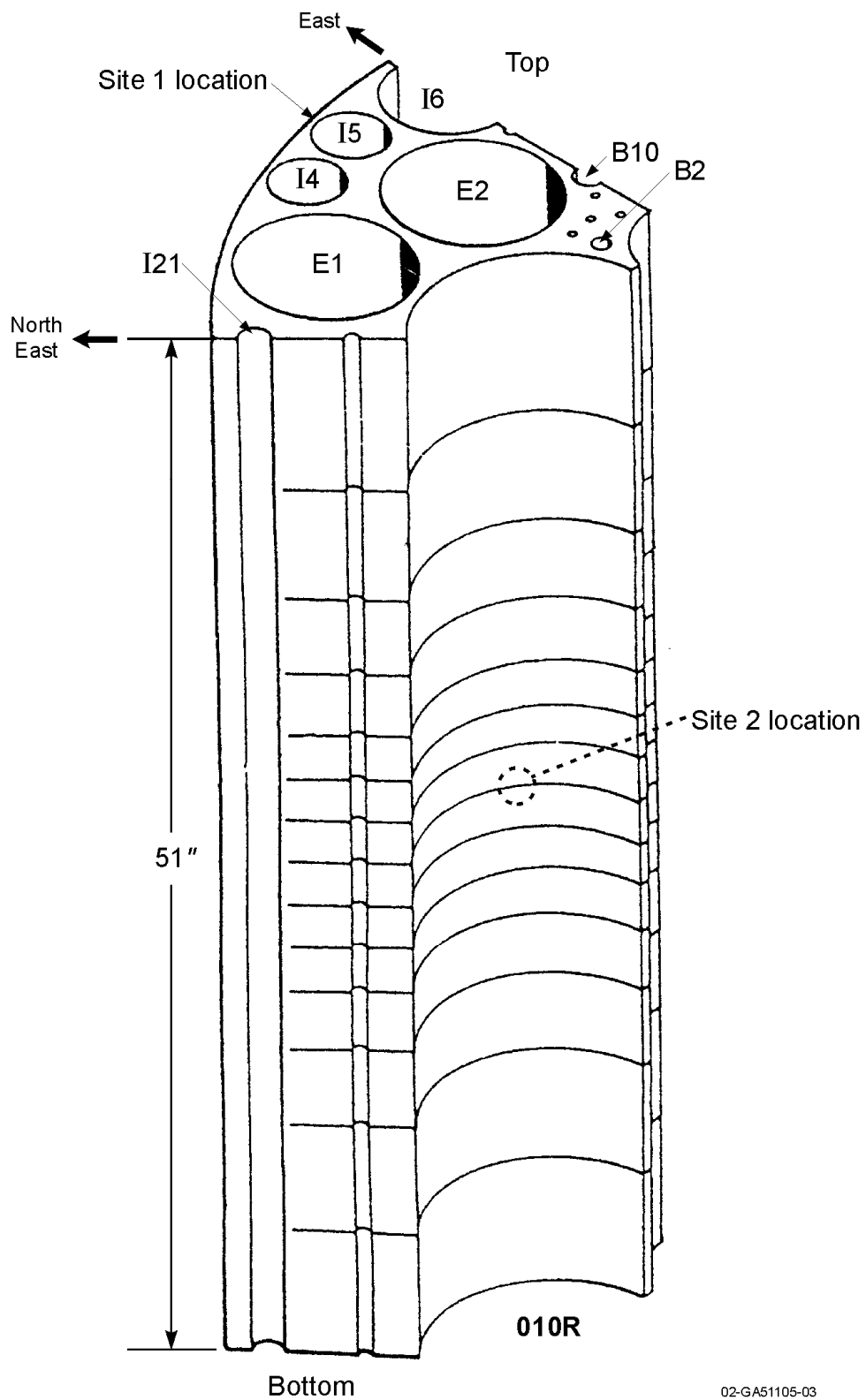


Figure 6-1. A schematic of Advanced Test Reactor reflector Block 010R showing the locations of sample Sites 1 and 2.

## 6.2 Computer Code Simulations

Three computer codes were used to estimate radionuclide inventories:

- MCNP4B (LANL 1997)
- ORIGEN2 (Croff 1980)
- MCNP4B-ORIGEN2 Coupled Utility Program Code (MOCUP) (Babcock et al. 1994).

These computer codes were used to develop the nuclear reaction cross sections and irradiation-flux levels as a function of position in the beryllium and to perform the activation analyses.

The MCNP4B computer code is a general purpose, continuous energy, generalized geometry, and coupled neutron-photon-electron Monte Carlo transport code. This code performs the neutron transport calculation to determine the flux and reaction rates in the geometry model cells and the desired neutron cross sections. A wide variety of nuclide cross-sections and reactions are available from the Evaluated Nuclear Data File-5 and -6.

ORIGEN2 (Croff 1980) is used for calculating the buildup, destruction, and decay of stable and radioactive isotopes. Coupled ordinary differential equations describing the complex burnup and decay mechanisms between the nuclides are solved using the matrix exponential method. Several standard neutron cross-section, decay, and production data libraries are available with the code for a narrow range of applications. A special feature of the ORIGEN2 code is a user option to modify the standard cross-section libraries with user-supplied cross sections, thereby allowing a burnup calculation to be reactor-specific. ORIGEN2 performs the burnup calculation with effective one-group cross sections with depletion controlled either by power or irradiation flux level.

MOCUP (Babcock et al. 1994) is a utility code composed of a system of external processors that link input and output files from the MCNP4B and ORIGEN2 codes. For characterization analyses, the MOCUP code was used only to transcribe neutron fluxes and nuclear reaction rates into one-group neutron cross sections for use in ORIGEN2. The MOCUP code is composed of three processing modules, namely, mcnpPRO, origenPRO, and compPRO. Each module performs specific, sequential tasks during each time step or burnup iteration.

## 6.3 Calculation Methodology

The calculation methodology uses mcnpPRO, origenPRO, and compPRO computer codes in a serial process. MCNP4B performs the neutronic transport calculation to determine the cell fluxes and reaction rates. MOCUP reads the MCNP4B output and arithmetically manipulates the data into one-group cross sections for input into ORIGEN2. To obtain the radionuclide concentrations, ORIGEN2 is then used to calculate the time-dependent, nuclide-coupled depletion or activation analysis. The ORIGEN2 calculation requires other input data in addition to the neutron cross-sections, as discussed below.

To perform the MCNP4B neutronic calculations, a geometric model of the ATR core is required. A full-core, fully explicit, three-dimensional geometrical and material model of the entire ATR core accounts for core axial and radial asymmetries. This model contains the major ATR core features, including the 40 driver fuel elements, nine flux trap facilities, safety rods, neck shim housing, shim control rods, 16 OSCCs, and the eight beryllium reflector blocks. The beryllium reflector blocks are modeled individually and can be subdivided further as was done for Site 1, Site 2, and the segmented three-dimensional model, to obtain cell-specific and location-specific neutron cross sections. A cross-sectional view of the MCNP4B

ATR core model is shown in Figure 6-2. Each colored section of Figure 6-2 represents a different region of the computer model. For example, the purple region represents the 40 curved fuel elements, the light-yellow cylinders are the beryllium metal contained within the 16 OSCCs (the adjacent black sections represent the hafnium plates), and the light-green area models the eight ATR beryllium blocks.

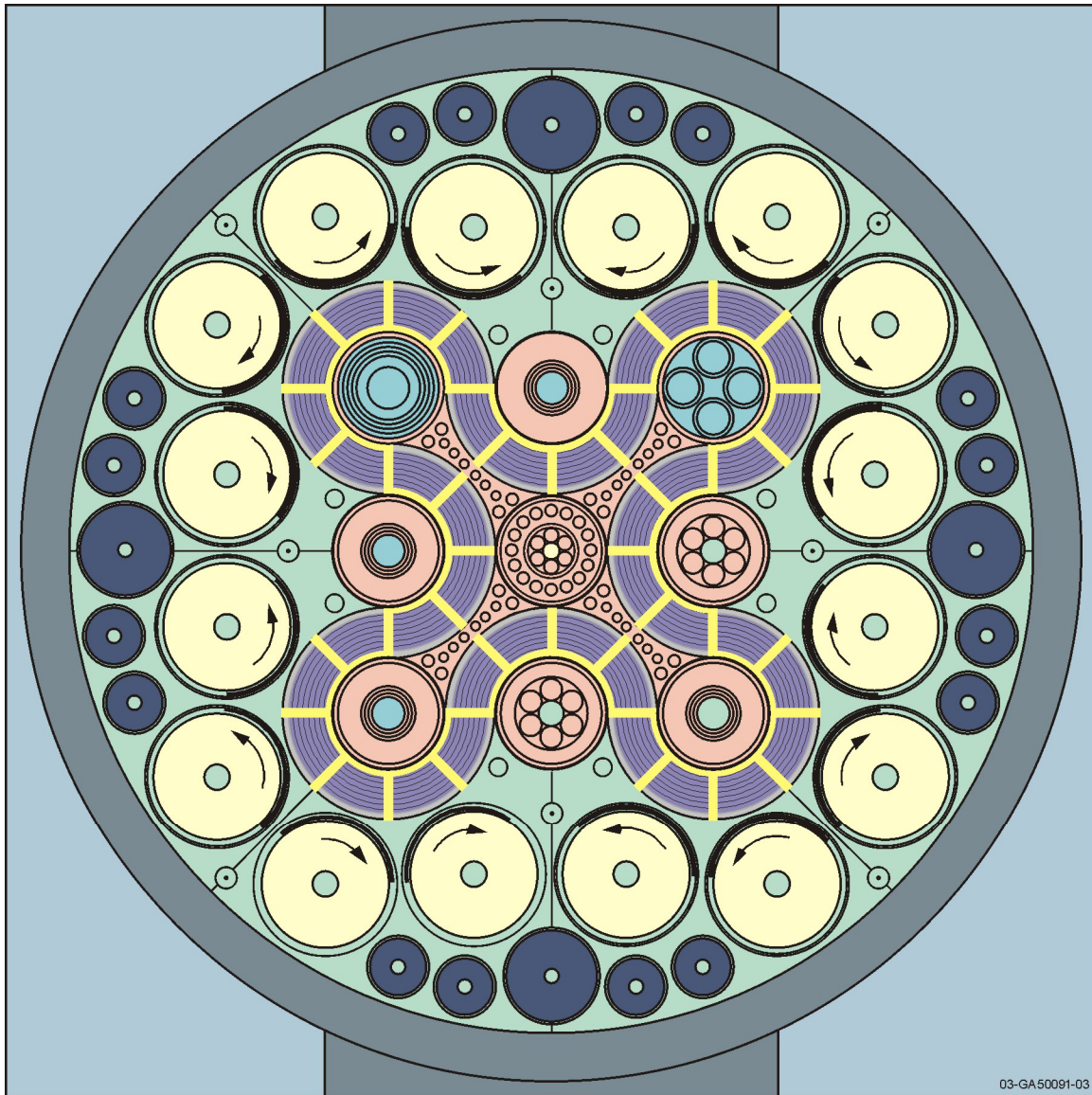


Figure 6-2. Cross-sectional view of the Monte Carlo N-Particle Version 4B Advanced Test Reactor full core model.

The nuclear reaction rates were calculated by MCNP4B for a variety of actinides and selected precursor activation products. Reaction rates were determined for 37 actinides, including 12 of the 13 important actinides that form the basis of the TRU waste definition, plus 24 selected activation product and precursor nuclides that also are included and given in Table 6-1.

For each of the 37 actinide nuclides, four nuclear reaction rates were calculated: (n,f), (n,  $\gamma$ ), (n,2n), and (n,3n). For the activation product nuclides, four nuclear reaction rates are calculated: (n, $\gamma$ ), (n,2n), (n, $\alpha$ ), and (n,p).

The ORIGEN2 code performed the activation analysis. In addition to the location-specific neutron cross sections, the irradiation flux and the beryllium block mass constituents were required as input data. The beryllium block irradiation flux is calculated by MCNP4B and normalized, based on the ATR lobe exposures. Table 6-2 below gives the ATR core total exposures for Cores 1 through 4, along with the corresponding operational dates and durations.

Table 6-1. List of actinide and activation product nuclides for which nuclear reaction rates are calculated by the Monte Carlo N-Particle Version 4B computer code.

Actinides	Activation Products
Th-232, Th-233	Li-6
Pa-233	Be-9
U-233, U-234, U-235, U-236, U-237, U-238, U-239, U-240	C-12, C-13
Np-235, Np-236, Np-237, Np-238	N-14
Pu-237, Pu-238, Pu-239, Pu-240, Pu-241, Pu-242, Pu-243	O-17
Am-241, Am-242m, Am-243	Co-59, Co-60, Co-60m
Cm-242, Cm-243, Cm-244, Cm-245, Cm-246, Cm-247, Cm-248,	Ni-58, Ni-59, Ni-60, Ni-61, Ni-62, Ni-63, Ni-64
Bk-249	Cu-63
Cf-249, Cf-250, Cf-251, Cf-252	Zn-66
	Nb-93, Nb-94
	Mo-94, Mo-98, Mo-99
	Tc-99

Table 6-2. Core data and total core exposures for the Advanced Test Reactor.

Advanced Test Reactor Core	Time Period	Duration (days)	Start and End Cycles	Approximate Number of Power Cycles	Total Core Exposure (MWd)
1	02/01/68 to 09/09/72	1,682	Initial Critical to 14A	45	141,240
2	02/05/73 to 04/11/77	1,526	15A to 34C1	64	153,734
3	08/09/77 to 02/02/86	3,098	35A7 to 72A1	120	305,241
4	05/18/86 to 02/27/94	2,843	73A9 to 102B1	90	267,247
5	07/11/94 to 08/07/04	3,680	103A1 to 133B1	79	287,600

For example, the 010R beryllium reflector block resided in the northeast (NE) lobe of Core 3. Table 6-3 gives four Core 3 lobe exposures. The NE lobe exposure was used to normalize the 010R block irradiation fluxes.

The mass constituents of the beryllium block (beryllium mass plus the assortment of impurity masses) also are important pieces of input data for the ORIGEN2 activation calculation. The beryllium constituent masses are based on reflector material and chemical impurity information previously provided. The accuracy of the beginning of life chemical impurities plays an important role in the quest to obtain an accurate activation analysis and prediction of radionuclide inventory. The three major input data—neutron cross sections, irradiation flux, and beryllium masses—are required for each activation analysis.

Table 6-3. Core 3 lobe exposure data.

Lobe	Irradiation Time (days)	Lobe Exposure (MWd)
NE	3,098	47,259
SE	3,098	72,984
SW	3,098	60,200
NW	3,098	53,920

NE = northeast  
NW = northwest  
SE = southeast  
SW = southwest

## 6.4 Five Activation Analyses

Five separate activation analyses estimated the neutron-induced radioactivity in the 010R beryllium block. These five analyses focused on (1) the whole beryllium block, (2) Site 1, (3) Site 2, (4) an OSCC, and (5) a segmented beryllium block. All five analyses relied on the same basic calculation methodology described above to develop location-specific neutron cross sections and irradiation fluxes. Location-specific cross sections and fluxes also were critical for accurate estimates of radionuclide activity, as was evident in the early comparisons of calculated versus measured radionuclide concentrations. All other input data (e.g., exposure history and chemical impurity masses) remained the same for the five cases analyzed.

Neutron reaction cross sections were needed for all five cases as part of the activation analysis input data. These data were generated using the Monte Carlo neutron transport code, MCNP4B, and a full ATR core model with explicit three-dimensional geometric detail. The model includes the 40 driver fuel elements, eight beryllium reflector blocks, one neck shim housing, nine flux traps, and 16 outer shim control cylinders (see Figure 6-2). In particular, the 010R beryllium reflector block located in the NE reflector lobe was specially subdivided to get the needed neutron fluxes and nuclear reaction rates at specific block locations (i.e., Site 1, Site 2, and OSCC).

The MCNP4B code has the capability to calculate neutron fluxes and nuclear reaction rates in any defined cell location in the model. Using this capability, the beryllium block cells in the ATR full model were modified to calculate fluxes and reaction rates in the cell regions representing the following:

1. Full beryllium block
2. Single low-flux location at the top periphery of the block (Site 1)

3. Single high-flux location on the front face of the block at mid-plane (Site 2)
4. An OSCC
5. A 330-cell fully segmented block.

With the cell fluxes and reaction rates, specific flux-collapsed one-group neutron cross sections could be calculated for activation product and actinide precursors. One-group reaction cross sections included fission, radioactive capture, (n,2n), (n,p), (n, $\alpha$ ), and (n,3n) reactions.

## 6.5 Assumptions

In making the calculations, the following assumptions are used:

- The activation analysis calculations pertain only to the beryllium metal pieces of the reflector blocks. All other nonberyllium components (e.g., pads, screws, nuts, dowels, and clamps) attached to the beryllium reflector blocks were not accounted for in the calculated and reported radionuclide inventory.
- All radionuclide activities were decay-corrected to July 15, 2001.
- An individual beryllium block volume is  $0.0447 \text{ m}^3$ . The entire block mass is 82.7 kg (or 81.4 kg for the beryllium metal only). The assumed beryllium density was  $1.85 \text{ g/cm}^3$ .
- Constant power and flux were assumed over each ATR power phase. For the 010R block, the estimated total neutron flux was  $1.342 \times 10^{14} \text{ n/cm}^2/\text{second}$ . The total irradiation time was 3,098 days. The decay time to July 15, 2001, was 5,642 days.
- Beryllium metal uranium impurity of 30 ppm was assumed to be uniformly distributed throughout the blocks.

## 6.6 Segmented Model

A segmented model of the 010R beryllium block was developed to determine the detailed distribution of the TRU concentrations throughout the block volume (see Figure 6-3). Because the previously calculated average block TRU concentrations were significantly higher than both the calculated and measured TRU concentrations at Sites 1 and 2, this meant that somewhere within the beryllium block the TRU concentrations were significantly higher than the average block value. This led to questions concerning how much higher and where in the block these potentially high TRU concentrations are located. These questions could be answered only with the segmented model and the associated detailed activation analysis.

The segmented model subdivides the 010R beryllium block into five radial and six azimuthal zones or 30 r- $\theta$  segments, as shown in Figure 6-3. Note, however, that only 22 of the 30 r- $\theta$  segments actually contain a piece of the beryllium reflector block metal. Some segments contained fuel and others were for OSCC locations. In addition, the beryllium block was further subdivided into 15 axial zones with 8-cm (3-in.) segment lengths, except for the two end segments, which had 17 cm (6.5 in.) and 14 cm (5.5 in.) lengths at the top and bottom of the block, respectively. In total, the beryllium block was divided into  $22 \times 15$  (or 330) individual segments.

As discussed above, the fluxes and cross sections were calculated for each of these 330 segments in the same manner as the fluxes and cross sections had been calculated for the Site 1, Site 2, OSCCs, and the entire block (average over the block). An individual activation analysis or ORIGEN2 run was performed for each of these 330 segments to obtain the radionuclide inventory of each segment. The results are discussed in the next section.

## 6.7 Results from Segmented Model

Computations used the methodology and computer codes discussed above to calculate the TRU-specific activities (nano-curies per gram) in each of the 330 segments. Each segment-specific activity is an average over the segment's volume. The 22 r- $\theta$  segment-specific activities are plotted in Figures 6-3 through 6-7 as a function of axial height above the bottom of the ATR active core. The location of the 22 segments corresponds to the 22 numbered segments on Figure 6-3. Figure 6-4 plots values for Segments 1 through 5, Figure 6-5 plots values for Segments 6 through 10, Figure 6-6 plots values for Segments 11 through 16, and Figure 6-7 plots values for Segments 17 through 22.

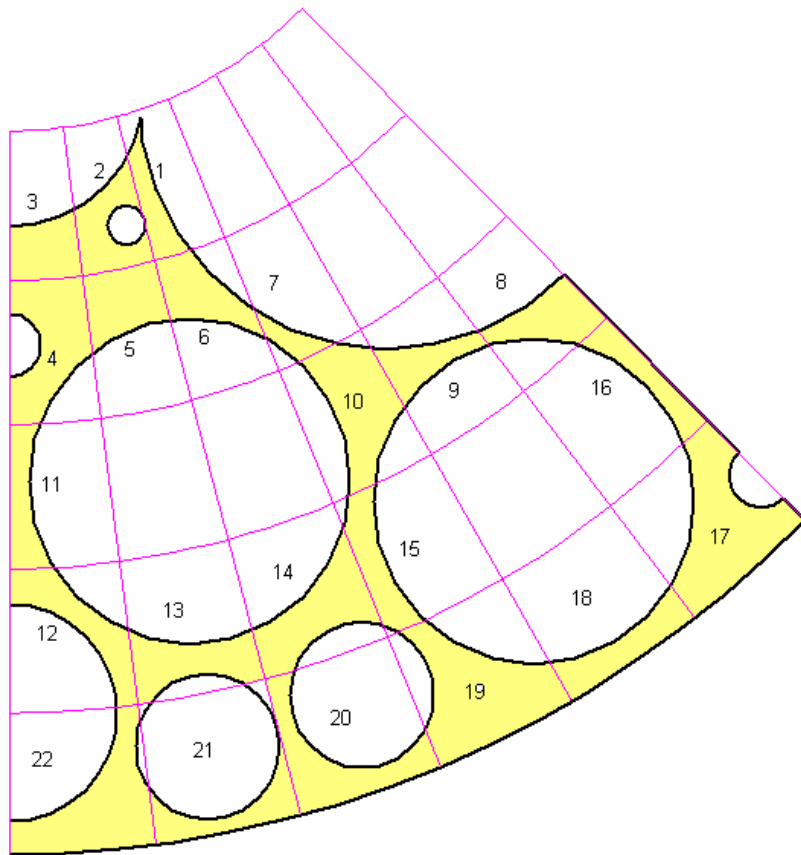


Figure 6-3. Segmentation of the Advanced Test Reactor beryllium reflector block used in the detailed calculations.



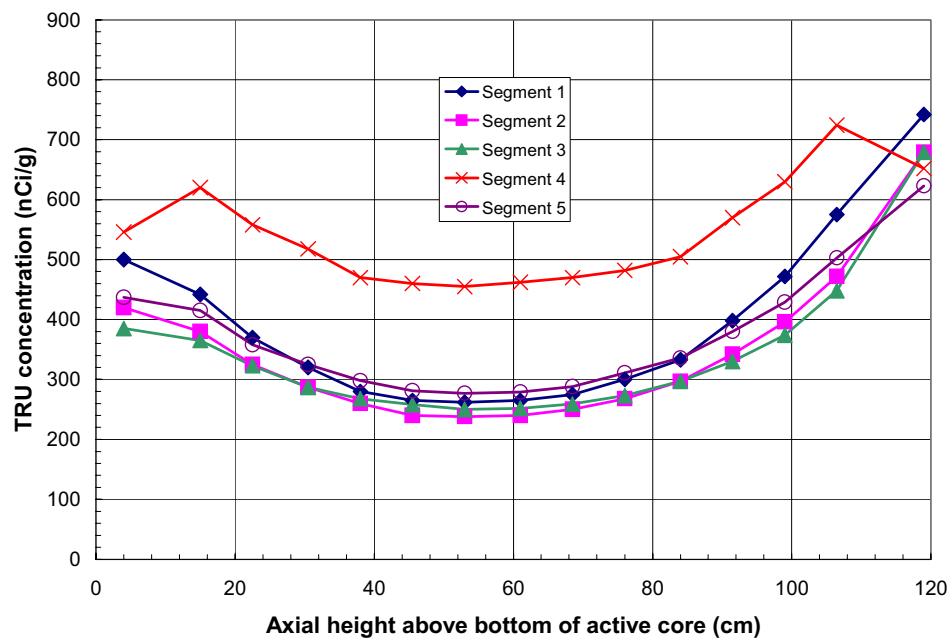


Figure 6-4. Transuranic specific activities calculated for Segments 1 through 5.

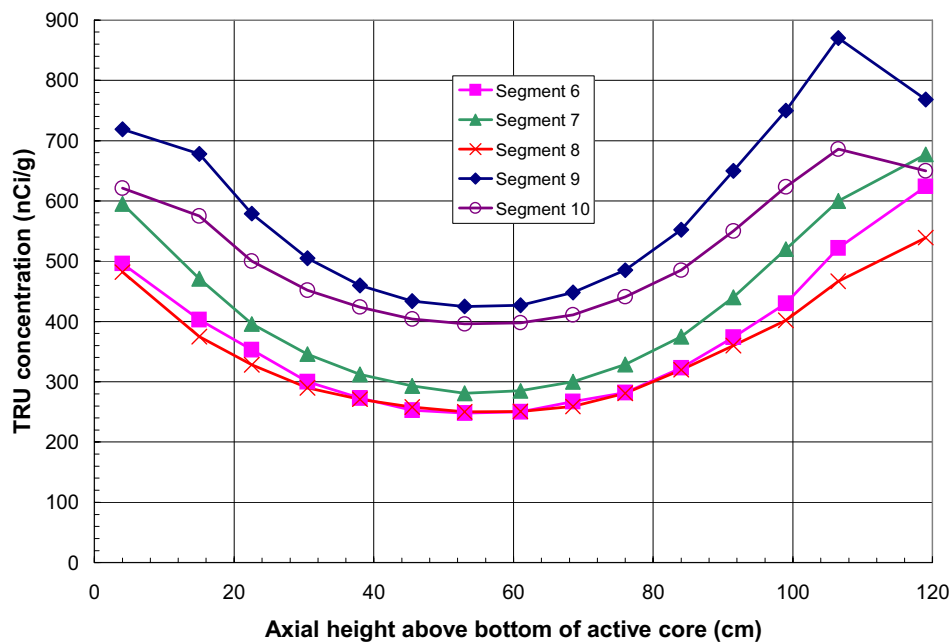


Figure 6-5. Transuranic specific activities calculated for Segments 6 through 10.

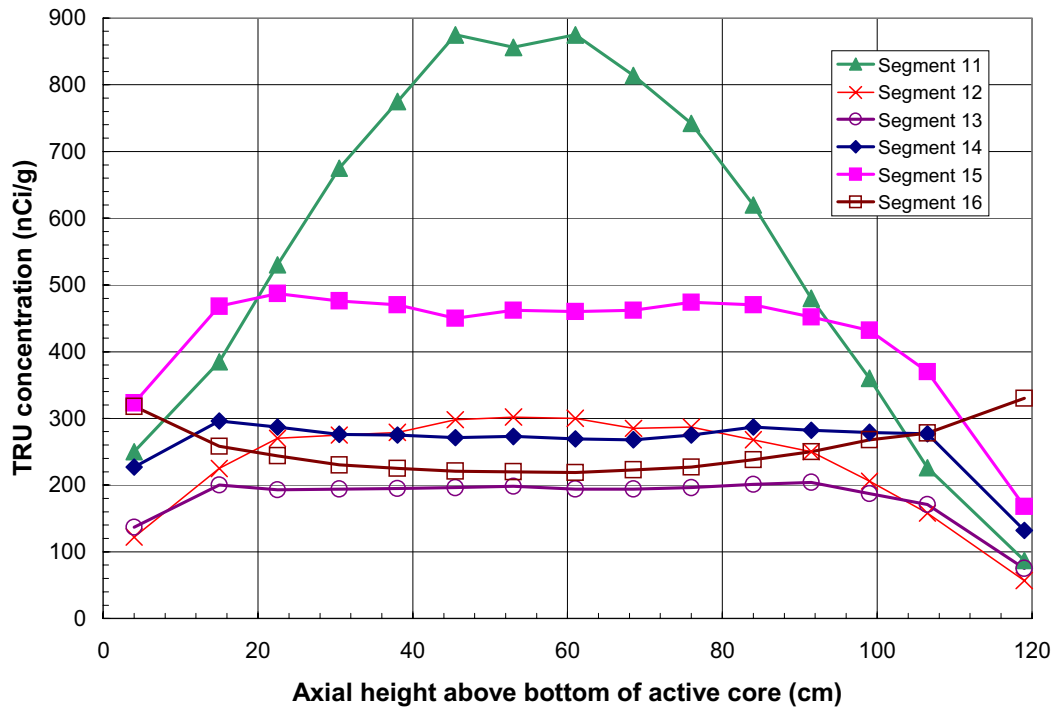


Figure 6-6. Transuranic specific activities calculated for Segments 11 through 16.

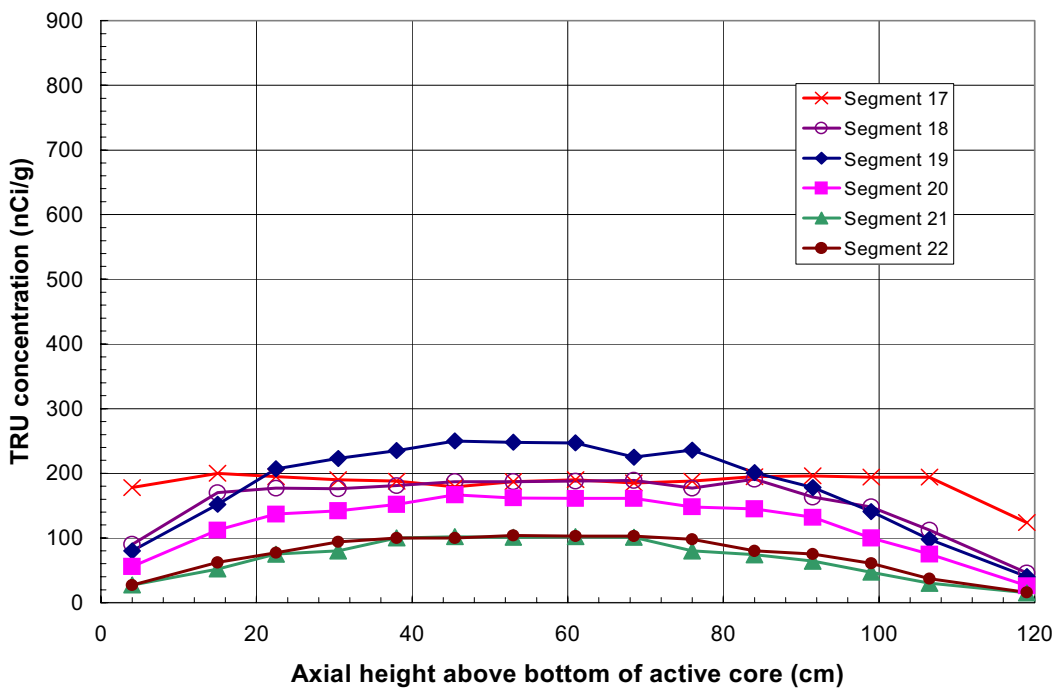


Figure 6-7. Transuranic specific activities calculated for Segments 17 through 22.

Figures 6-4 through 6-7 were surveyed to see which segments had the highest and lowest TRU concentrations. Segments 9 (near top of the active core) and 11 (around core midplane) appear to have the highest TRU concentrations at approximately 890 nCi/g. Note also that the TRU concentrations in Segments 1 through 10 show a depression in the axial profile around midplane and peaking near the top and bottom of the core. The depression is believed to be the result of the higher midplane neutron fluxes in the vicinity of the driver fuel resulting in increased burnout of the uranium and TRU isotopes. Segments near the block outer periphery exhibit the lowest TRU concentrations, presumably because of the reduced neutron fluence. Apparently, an optimal neutron flux intensity and spectral content can maximize the TRU concentration in the beryllium block, as evidenced by the variation in the plots.

Table 6-4 shows a comparison of Pu-239 and TRU concentrations based on the segmented model calculation, a single average block, and measured assay data for Site 1, Site 2, and the block average. The single-block model uses a single calculated average flux and cross-section set. Note that all the beryllium block radionuclide inventories to date are based on this type of model. The segmented model represents a more detailed and accurate computation, but is by far more complex and time consuming, and hence limiting, in the sense that only the 010R block was analyzed.

A comparison between results of the segmented model and the single-block model indicates good agreement, particularly at Sites 1 and 2 for both the Pu-239 and TRU concentrations. The Pu-239 measured value for Sites 1 and 2 are in very good agreement with both calculated values, as well. The measured TRU value at Site 2, however, is higher than the segmented model calculated values by a factor of 1.52 and 1.86 (corresponding to the two measured samples at Site 2). These factors are within a factor of two and demonstrate good agreement. Of particular interest is the underprediction of measured TRU values at Site 2 by both the segmented model and the single-block model.

Table 6-4. Calculated and measured Pu-239 and transuranic concentrations.

Sample Locations for Block 010R	Concentration of Pu-239 (nCi/g)	Concentration of All Transuranic Isotopes (nCi/g)
Site 1		
Segmented model <sup>a</sup>	6.353	13.719
Single-block model	5.119	8.56
Measured	4.4	Not measured
Site 2		
Segmented model <sup>b</sup>	11.98	286.46
Single-block model	11.71	279.50
Measured	14.9 and 13.0	434.8 and 533.4
Block average		
Segmented model	Not measured	277.08
Single-block model	Not measured	491.23
Measured	Not measured	Not measured

a. Site 1 is in cell-20123 of the segmented model.  
b. Site 2 is in cell-20807 of the segmented model.

Table 6-5 presents the fraction of the 010R block mass that exceeds different levels of specific activity. For example, approximately 97% of the beryllium block mass has TRU concentrations in excess of 100 nCi/g and nearly 50% of the block mass is in excess of 400 nCi/g.

Other useful information derived from the segmented model includes total TRU activity inventory, which is estimated to be 0.0277 Ci. The segmented model calculations also predict an overall block average TRU concentration of 277.08 nCi/g versus the 491.23 nCi/g that is computed for the single-block (ORIGEN2) model. This comparison indicates that the single-block (one-dimensional) ORIGEN2 model may overpredict TRU concentrations by a factor of about 1.8 (relative to the three-dimensional model). However, other comparisons, based on measured data and computer code results (see Section 7.6) for Sites 1 and 2, indicate the opposite effect. That is, the single-block calculations tend to underpredict the block inventories by a factor of about 1.7. Since the computer code results are only known within a factor of 2, and because the above two effects tend to cancel each other, no additional correction was attempted to better refine the single-block ORIGEN2 inventory results. In other words, the reported single-block ORIGEN2 results are considered to be best estimate.

Table 6-5. Percentage of beryllium block mass exceeding a given specific activity level.

Specific Activity Level (nCi/g)	Percentage of Beryllium Block Mass Exceeding a Given Specific Activity Level (%)
>100	96.67
>200	81.70
>300	58.85
>400	48.62
>500	30.76
>600	20.92
>700	6.67
>800	2.06
>900	0.00

## 7. DESCRIPTION OF OAK RIDGE ISOTOPE GENERATION AND DEPLETION CODE VERSION 2 MODEL

This section describes the ORIGEN2 computer model and the calculated results for the radionuclide inventory in beryllium metal disposed of in the SDA from ATR, ETR, and MTR.

### 7.1 Background Information for the Advanced Test Reactor

The ATR reactor core contains eight reflector blocks and 16 OSCCs. The relative position of the beryllium components is shown in Figures 7-1 through 7-3. Each core configuration is composed of two reflector blocks and four OSCCs per lobe. The four outer lobes of the reactor are identified as NE, northwest (NW), southeast (SE), and southwest (SW). Looking from the center of the core outward, each lobe is split into two parts, a left side and a right side. For example, the block in the right side of the NE lobe is identified as NE-R. In Core 3 (see Figure 7-3), the block in position NE-R has the serial number 010R. The actual serial number engraved on this block is 010. The “R” is not a part of the block’s serial number, but is included to distinguish between left and right blocks with the same three-digit number. For example, Block 018 in Core 3 (e.g., 018L in NW-L) has the same three-digit serial number as Block 018 in Core 4 (e.g., 018R in SW-R). Another example is the blocks located in NE-L and SE-R of Core 4. In this last case, both blocks have the same serial number 017 and could not be distinguished from each other unless the “L” or “R” identifier is included with its serial number.

Note that in some documents, the position of a specific beryllium block in the ATR core might be described in different terms. For instance, Block 010R in NE-R (Core 3) might be referred to as east-right, or the block in reactor position number 2, or the block at location E1E2 (where E1 and E2 represent the OSCC positions within this block). See Figures 7-1 through 7-3 for the general relationship describing these various types of notation. The notation that is used in the following analysis is the lobe position (NW, NE, SE, or SW) followed by a left (L) or right (R) identifier. In many cases, the serial numbers of buried blocks are not known. For example, based on Figure 7-2, the beryllium block in Core Position No. 1 (e.g., N3N4) of Core 2 is identified as Block NE-L with no serial number. The block that was in the reactor at this location was disposed of in the SDA and did have a serial number, but this information has been lost. Because the serial number of this particular block is not known, any reference to it is made based on its core and lobe position.

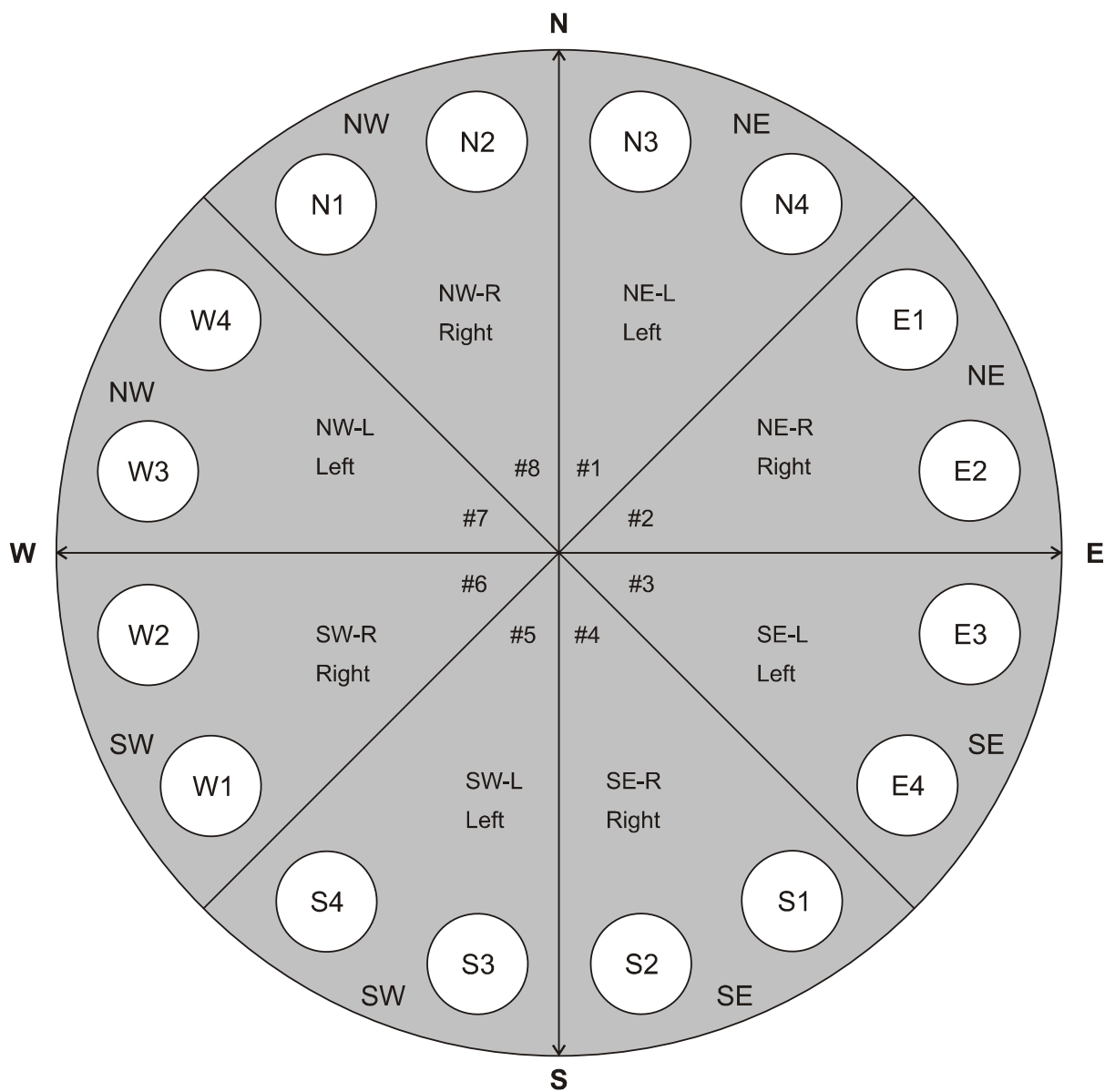
Though the ATR beryllium blocks do have serial numbers, the identity of those blocks from Core 1 has been lost. The position of six of the blocks disposed of from Core 2 (see Figure 7-2) also has been lost. The two blocks (i.e., 11R and 15L) from Core 2, and shown in Figure 7-2, currently reside in the canal. These two blocks are known to have come from Core 2 because they lack saw cuts on their exterior surfaces. Though the blocks from Core 1 also did not have saw cuts, it is known that Blocks 11R and 15L could not have come from Core 1 since all blocks from Core 1 were disposed of in the SDA on or about December 1, 1976. Note that horizontal saw cuts were machined into the beryllium blocks that were placed in Cores 3, 4, and 5. These saw cuts were made to relieve stress resulting from internal gas buildup.

The SDA disposal records indicate that the ATR beryllium blocks and OSCCs were disposed of during the following four campaigns:

- November through December 1976—eight blocks from Core 1 and no OSCCs
- October 1982—six blocks from Core 2 and no OSCCs (two blocks having no saw cuts still reside in the canal from Core 2)

- August through September 1987—nine OSCCs were disposed of (all from the Cores 1 and 2 irradiation period)
- May through July 1993—six blocks from Core 3 and no OSCCs.

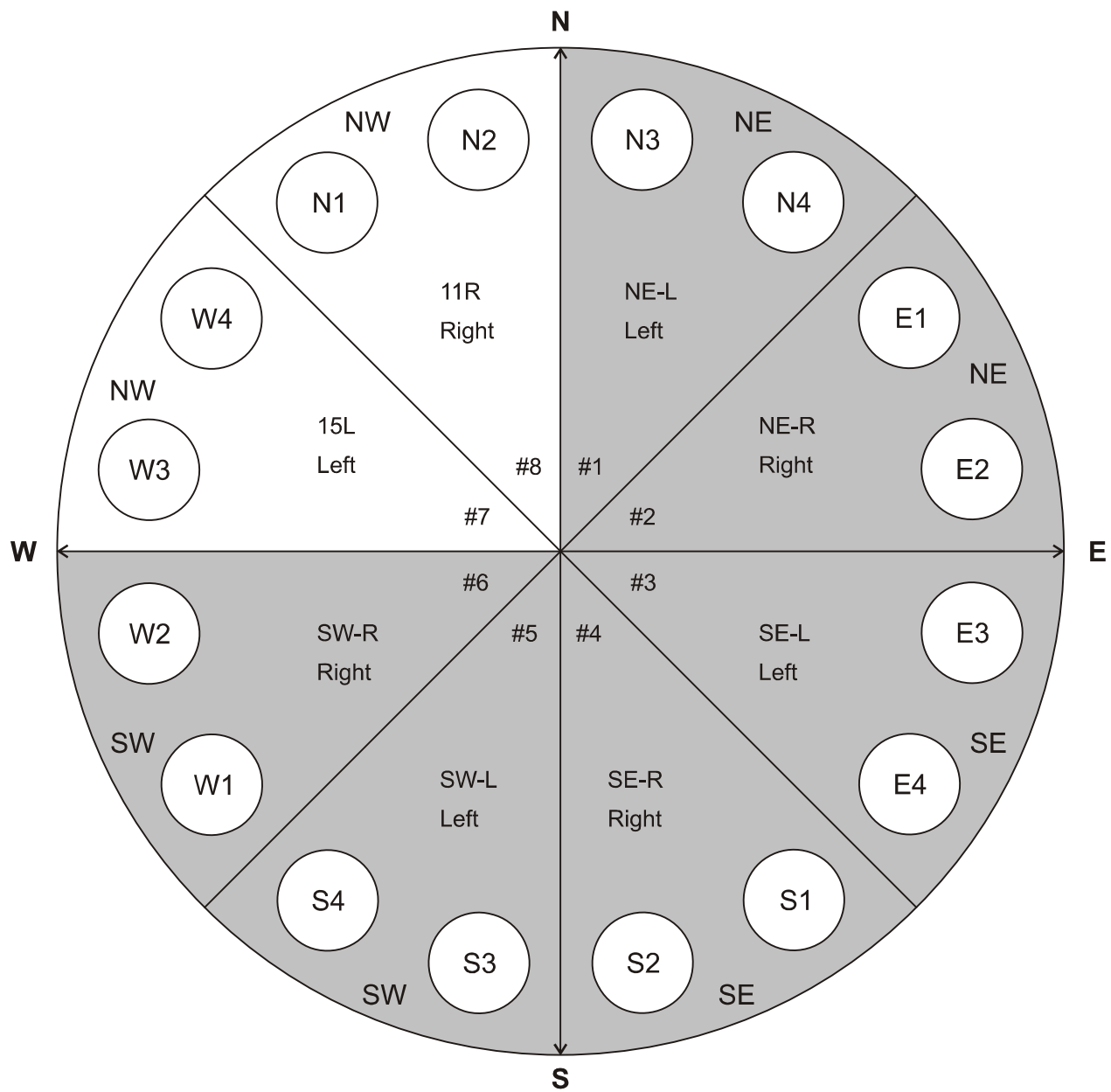
A total of 20 blocks and nine OSCCs were disposed of in the SDA from 1976 through 1993. A total of 20 blocks (eight from Core 5, eight from Core 4, two from Core 3, and two from Core 2) and 55 OSCCs currently remain in the ATR canal.



All blocks for Core 1 were disposed of in the Subsurface Disposal Area on or about December 1, 1976.

The serial numbers for the buried blocks and their specific loading configuration is not known.

Figure 7-1. Beryllium reflector loading for Core 1, Advanced Test Reactor.

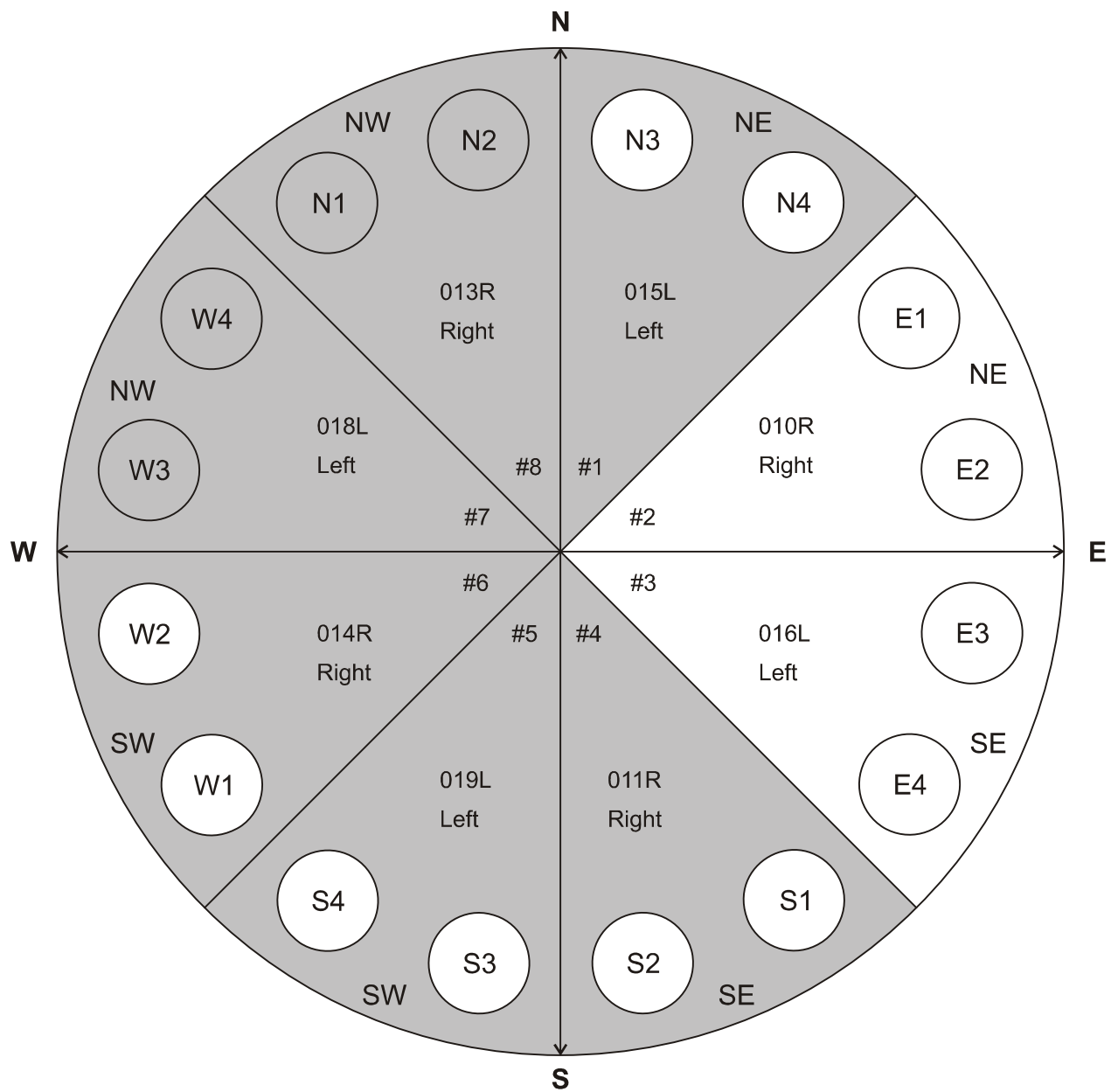


G1532-01

Shaded blocks were disposed of in the Subsurface Disposal Area on or about October 14, 1982.

Figure 7-2. Estimated beryllium reflector loading for Core 2, Advanced Test Reactor.

Note: All blocks from this core, except for those in the NW lobe, were disposed of in the SDA around October 14, 1982. Serial numbers of the six blocks disposed of are not known. Blocks 11R and 15L remain in the ATR canal. The irradiation positions for 11R and 15L are assumed to be from the NW lobe, but this is not certain.



G1532-02

Shaded blocks were disposed of in the Subsurface Disposal Area on or about July 1, 1993.

Figure 7-3. Beryllium reflector loading for Core 3, Advanced Test Reactor.

Note: Six of the eight blocks from Core 3 were disposed of in the SDA around July 1, 1993. Blocks 010R and 016L remain in the ATR canal. The core positions of all blocks in Core 3 are known.



All of these blocks and OSCCs from Core 4 and Core 5 are in the ATR canal. None were disposed of. The core positions of all blocks from Cores 4 and 5 are known.

Fifty-five OSCCs remaining in the canal result from the following activities:

- Seven from irradiation of Cores 1 and 2
- Sixteen from Core 3
- Sixteen from Core 4
- Sixteen from Core 5.

Note that OSCCs from Core 1 were reused in Core 2, but the beryllium blocks were not reused. A total of 40 blocks and 64 OSCCs were irradiated from Cores 1 through 5 (eight blocks from each core), and 16 OSCCs from each of four cores (2, 3, 4, and 5). However, specific block serial numbers and reactor positional information were not recorded during each disposal campaign. Therefore, the exact disposal dates of each block or OSCCs are not known because shipments were made over several months. To simplify computer analysis, ORIGEN2 calculations used decay times computed to average disposal dates for each major campaign. For example, December 1, 1976, was used for eight blocks disposed of from Core 1. October 14, 1982, was used for six blocks disposed of from Core 2. September 1, 1987, was used for nine OSCCs disposed of from Cores 1 and 2. July 1, 1993, was used for six blocks disposed of from Core 3. In addition to these disposal dates, all calculations were decayed out to September 15, 2001. This date represents a common reference point, which happens to approximate the time at which the first set of measured TRU data was received from MFC for Block 010R. The common decay time also allows all results to be compared against the same time instead of different disposal time periods.

Two of the 20 reflector blocks in the canal are of Core 1 or 2 design. These two reflector blocks can be distinguished from newer blocks by the presence of 36 cooling holes and the absence of saw cuts. No specific documentation has been found that identifies what quadrant (i.e., lobe) in which these blocks were installed, nor whether either or both came from Core 1 or from Core 2; however, based on their high serial numbers, it is likely that these reflector blocks came from Core 2. For modeling purposes, the position of two blocks remaining in the canal was assumed to be from the NW lobe of Core 2 (as shown in Figure 7-2); however, their exact location is not certain. This means that the six blocks disposed of from Core 2 are postulated to come from the NE, SE, and SW lobes.

## **7.2 Advanced Test Reactor Power History**

Basic irradiation history, average power data, total neutron flux, core configuration, and disposal (decay) dates are shown in Table 7-1. Data in Table 7-1 apply to all of the 40 beryllium blocks that were used during the last five core loadings. Information on OSCCs is not explicitly shown in Table 7-1; however, OSCC data are linked with specific reflector blocks that contained them and can be determined using data from reflector blocks. OSCC data can be determined from Table 7-1 with the knowledge that the nine OSCCs disposed of came from Core 2, but also were irradiated during Core 1. That is, reflector blocks from Core 1 were removed during the first core changeout, and a new set of reflector blocks were installed in Core 2, but 16 OSCCs from Core 1 were reused in Core 2. Therefore, the first set of OSCCs saw two short core irradiations while the reflector blocks were removed during each changeout. Consequently, during the five core irradiation periods, ATR has had 40 blocks ( $8 \times 5$ ) and 64 OSCCs ( $16 \times 4$ ) removed. However, only 20 blocks and nine OSCCs have been disposed of in the SDA.

Table 7-1. Irradiation history and reactor power data for the Advanced Test Reactor beryllium blocks disposed of from Cores 1, 2, 3, 4, and 5.

Block Serial Number or Core Position	EG&G <sup>a</sup> Material Number	Core Loading	Initial Irradiation Date	Final Core Irradiation Date	Location	Modeled Disposal Date	Reactor Operation (days)	Total Core (MWd)	Lobe (MWd)	Average Block Total Flux	Average (MW)
<b>Blocks in the Canal</b>											
15L <sup>b</sup> no saw cuts	Unknown	2	2/5/1973	4/11/1977	ATR canal	Not disposed of	1,526	141,240	27,895	1.6083E+14	18.28
11R <sup>b</sup> no saw cuts	Unknown	2	2/5/1973	4/11/1977	ATR canal	Not disposed of	1,526	153,734	30,362	1.7506E+14	19.90
010R	Unknown	3	8/9/1977	2/2/1986	ATR canal	Not disposed of	3,099	305,241	47,259	1.3417E+14	15.25
016L	023	3	8/9/1977	2/2/1986	ATR canal	Not disposed of	3,099	305,241	72,984	2.0720E+14	23.55
015R	022	4	5/18/1986	2/27/1994	ATR canal	Not disposed of	2,842	267,247	41,565	1.2868E+14	14.63
016R	023	4	5/18/1986	2/27/1994	ATR canal	Not disposed of	2,842	267,247	41,883	1.2966E+14	14.74
017L	024	4	5/18/1986	2/27/1994	ATR canal	Not disposed of	2,842	267,247	41,883	1.2966E+14	14.74
017R	024	4	5/18/1986	2/27/1994	ATR canal	Not disposed of	2,842	267,247	68,710	2.1271E+14	24.18
018R	021	4	5/18/1986	2/27/1994	ATR canal	Not disposed of	2,842	267,247	57,389	1.7766E+14	20.19
020L	026	4	5/18/1986	2/27/1994	ATR canal	Not disposed of	2,842	267,247	68,710	2.1271E+14	24.18
021L	027	4	5/18/1986	2/27/1994	ATR canal	Not disposed of	2,842	267,247	57,389	1.7766E+14	20.19
022L	028	4	5/18/1986	2/27/1994	ATR canal	Not disposed of	2,842	267,247	41,565	1.2868E+14	14.63
NW-L		5	7/11/1994	08/07/04	ATR canal	Not disposed of	3680	287,600	44,920		12.21
NW-R		5	7/11/1994	08/07/04	ATR canal	Not disposed of	3680	287,600	44,920		12.21
NE-L		5	7/11/1994	08/07/04	ATR canal	Not disposed of	3680	287,600	47,172		12.82
NE-R		5	7/11/1994	08/07/04	ATR canal	Not disposed of	3680	287,600	47,172		12.82
SW-L		5	7/11/1994	08/07/04	ATR canal	Not disposed of	3680	287,600	61,786		16.79
SW-R		5	7/11/1994	08/07/04	ATR canal	Not disposed of	3680	287,600	61,786		16.79
SE-L		5	7/11/1994	08/07/04	ATR canal	Not disposed of	3680	287,600	70,270		19.10
SE-L		5	7/11/1994	08/07/04	ATR canal	Not disposed of	3680	287,600	70,270		19.10
<b>Blocks in the SDA</b>											
	Lobe										
NW-L	NW	1	2/1/1968	9/9/1972	SDA	12/01/76	1,682	141,240	28,894	1.5114E+14	17.178
NW-R	NW	1	2/1/1968	9/9/1972	SDA	12/01/76	1,682	141,240	28,894	1.5114E+14	17.178
NE-L	NE	1	2/1/1968	9/9/1972	SDA	12/01/76	1,682	141,240	27,967	1.4629E+14	16.627
NE-R	NE	1	2/1/1968	9/9/1972	SDA	12/01/76	1,682	141,240	27,967	1.4629E+14	16.627
SW-L	SW	1	2/1/1968	9/9/1972	SDA	12/01/76	1,682	141,240	27,978	1.4635E+14	16.634

Table 7-1. (continued).

Block Serial Number or Core Position	EG&G <sup>a</sup> Material Number	Core Loading	Initial Irradiation Date	Final Core Irradiation Date	Location	Modeled Disposal Date	Reactor Operation (days)	Total Core (MWd)	Lobe (MWd)	Average Block Total Flux	Average (MW)
SW-R	SW	1	2/1/1968	9/9/1972	SDA	12/01/76	1,682	141,240	27,978	1.4635E+14	16.634
SE-L	SE	1	2/1/1968	9/9/1972	SDA	12/01/76	1,682	141,240	28,017	1.4655E+14	16.657
SE-R	SE	1	2/1/1968	9/9/1972	SDA	12/01/76	1,682	141,240	28,017	1.4655E+14	16.657
NE-L	NE	2	2/5/1973	4/11/1977	SDA	10/14/82	1,526	153,734	23,625	1.3621E+14	15.482
NE-R	NE	2	2/5/1973	4/11/1977	SDA	10/14/82	1,526	153,734	23,625	1.3621E+14	15.482
SW-L	SW	2	2/5/1973	4/11/1977	SDA	10/14/82	1,526	153,734	36,285	2.0920E+14	23.778
SW-R	SW	2	2/5/1973	4/11/1977	SDA	10/14/82	1,526	153,734	36,285	2.0920E+14	23.778
SE-L	SE	2	2/5/1973	4/11/1977	SDA	10/14/82	1,526	153,734	24,357	1.4043E+14	15.961
SE-R	SE	2	2/5/1973	4/11/1977	SDA	10/14/82	1,526	153,734	24,357	1.4043E+14	15.961
018L	NW	3	8/9/1977	2/2/1986	SDA	07/01/93	3,099	305,241	53,924	1.5309E+14	17.400
013R	NW	3	8/9/1977	2/2/1986	SDA	07/01/93	3,099	305,241	53,924	1.5309E+14	17.400
015L <sup>b</sup>	NE	3	8/9/1977	2/2/1986	SDA	07/01/93	3,099	305,241	47,259	1.3417E+14	15.250
019L	SW	3	8/9/1977	2/2/1986	SDA	07/01/93	3,099	305,241	60,205	1.7092E+14	19.427
014R	SW	3	8/9/1977	2/2/1986	SDA	07/01/93	3,099	305,241	60,205	1.7092E+14	19.427
011R	SE	3	8/9/1977	2/2/1986	SDA	07/01/93	3,099	305,241	72,984	2.0720E+14	23.551

ATR = Advanced Test Reactor

L = left

MW = megawatt

MWd = megawatt-day

NE = northeast

NW = northwest

R = right

RWMC = Radioactive Waste Management Complex

SDA = Subsurface Disposal Area

SE = southeast

SW = southwest

a. EG&amp;G Idaho is a former contractor operator at the Idaho National Laboratory.

b. Blocks 11R and 011R, as well as 15L and 015L, represent different serial numbers and different blocks.

Other key information needed to complete computer modeling of the reflector blocks and OSCCs are (1) elemental composition of the beginning-of-life condition of the beryllium metal used in ATR components, and (2) best-estimate neutron cross sections that apply to this material. Assumed elemental composition of disposed of ATR beryllium is shown in Table 7-2. This information is discussed in the next section. Cross-section data were obtained from MCNP4B calculations discussed in Section 6.

OSCCs were modeled using information shown in Table 7-1 for Core-1 reflector blocks. OSCC operational data were determined as follows. All nine OSCCs disposed of in 1987 came from the Cores 1 and 2 irradiation period. However, Cores 1 and 2 contained 16 OSCCs. Because it is not known which nine of the 16 OSCCs were sent to disposal, 9/16 of the entire Core 1 and 2 inventory were assumed to be disposed of. That is, an ORIGEN2 model was constructed for an entire core loading of 16 OSCCs. These OSCCs were irradiated from February 1, 1968, to September 9, 1972, (during Core 1), decayed to February 5, 1973, (the startup of Core 2), and then irradiated to April 11, 1977 (during Core 2). These results were then decayed to September 1, 1987, the assumed disposal date for the nine OSCCs, and also decayed to September 15, 2001, the common reference time period.

### **7.3 Elemental Composition of Beryllium from the Advanced Test Reactor**

Chemical composition (both primary and trace elements) of ATR beryllium blocks and OSCCs was determined from a variety of sources. In general, material composition data were determined from measured data obtained at MFC on beryllium samples collected from reflector blocks that currently reside in the ATR canal, or from chemical assay data reported by KBI on test reports for ATR beryllium, or from Brush Wellman chemical assay data obtained on recently purchased beryllium components. KBI datasheets (see Appendix A) were an important source of information on ATR beryllium material for ATR reflector blocks and OSCCs that were manufactured for Cores 1, 2, and 3. Presently, Brush Wellman is the supplier of all newly acquired ATR beryllium components (both blocks and OSCCs), components from Core 5 and components that reside in the reactor today (Core 6), and probably is the supplier of some beryllium components for Core 4. The chemical composition of beryllium metal varies depending on the original source of the beryllium ore. Unfortunately, older KBI chemical assay data are not sufficiently detailed to define all trace impurities that occur in ATR metal. For example, KBI datasheets do not report any information on either nitrogen or uranium, though both elements have been measured at MFC on KBI beryllium samples obtained from 12 ATR reflector blocks from Cores 2, 3, and 4 that are still in the canal. Consequently, supplementing KBI chemical assay data with either measured data or information from Brush Wellman was necessary to obtain a more complete elemental description of beryllium from ATR.

Measured data on ATR beryllium as reported by MFC are shown in Appendix B. MFC data were the primary source of information for the following elements: carbon, nitrogen, cobalt (Co-59 was estimated based on the measured Co-60 concentration), niobium, and uranium. KBI assay data were the primary source of information on many elements that were not measured in the MFC analysis, but were reported in KBI datasheets. To estimate concentrations of elements that were neither reported by KBI nor measured at MFC (or those elements that were only listed with limit-of-detection values), chemical assay information from Brush Wellman was used to supplement KBI data. Therefore, Brush Wellman was the third source of elemental information on ATR beryllium. Finally, in some cases when no data could be identified, limit of detection information was assumed. For example, lithium is an element that has neither been measured by MFC, nor is it reported by either KBI or Brush Wellman; however, a detection limit of less than 1.0 ppm is reported by KBI and a value of less than 3.0 has been reported by Brush Wellman. Therefore, for the case of buried ATR beryllium (which consists of KBI beryllium metal), lithium impurity concentration was assumed to be 1.00 ppm (by weight). Determination of the best-estimate elemental impurity data from the three individual data sets is illustrated in Table 7-2. The table also provides the best-estimate elemental composition for a typical ATR beryllium block (i.e., beryllium

material only), as well as average elemental assay data from beryllium materials manufactured by KBI and Brush Wellman. KBI data were obtained from data shown in Appendix A. Best-estimate elemental impurity information also is repeated in Table 7-3 with elemental mass composition for an ATR reflector block and an OSCC.

Table 7-2. Elemental composition data for beryllium from the Advanced Test Reactor.

Atomic Number	Atomic Weight	Symbol	Element Name	ATR Beryllium (ppm by wt)	MFC (ppm by wt)	KBI Data (ppm by wt)	Brush Wellman (ppm by wt)
1	1.0079	H	Hydrogen	—	—	—	—
2	4.0026	He	Helium	—	—	—	—
3	6.9410	Li	Lithium	1.000	—	<1.000	<3.000
4	9.0122	Be	Beryllium	980667.835	—	980670.935	989390.909
5	10.8110	B	Boron	1.917	—	1.917	1.880
6	12.0110	C	Carbon	745.000	745.000	725.000	973.636
7	14.0067	N	Nitrogen	205.400	205.400	—	229.913
8	15.9994	O	Oxygen	12618.667	—	12618.667	7088.727
9	18.9984	F	Fluorine	69.167	—	69.167	35.700
10	20.1797	Ne	Neon	1425.000	—	—	1425.000
11	22.9898	Na	Sodium	0.874	—	—	0.874
12	24.3050	Mg	Magnesium	45.000	—	45.000	203.182
13	26.9815	Al	Aluminum	355.833	—	355.833	357.864
14	28.0855	Si	Silicon	364.167	—	364.167	287.955
15	30.9738	P	Phosphorus	50.000	—	—	50.000
16	32.0660	S	Sulfur	7.500	—	—	<7.500
17	35.4527	Cl	Chlorine	50.000	—	<50.000	15.000
18	39.9480	Ar	Argon	6.370	—	—	6.370
19	39.0983	K	Potassium	13.070	—	—	13.070
20	40.0780	Ca	Calcium	200.000	—	<200.00	<20.000
21	44.9559	Sc	Scandium	2.300	—	2.300	<4.000
22	47.8800	Ti	Titanium	61.667	—	61.667	62.045
23	50.9415	V	Vanadium	3.423	—	—	3.423
24	51.9961	Cr	Chromium	92.500	—	92.500	86.114
25	54.9381	Mn	Manganese	56.667	—	56.667	87.714
26	55.8470	Fe	Iron	1499.167	—	1499.167	790.545
27	58.9332	Co	Cobalt	12.000	12.000	<12.000	7.893
28	58.6900	Ni	Nickel	225.833	—	225.833	108.864
29	63.5460	Cu	Copper	87.500	—	87.500	42.541
30	65.3900	Zn	Zinc	13.000	—	<100.000	<13.000
31	69.7230	Ga	Gallium	0.859	—	—	0.859
32	72.6100	Ge	Germanium	5.000	—	—	5.000
33	74.9216	As	Arsenic	1.782	—	—	1.782
34	78.9600	Se	Selenium	2.383	—	—	2.383
35	79.9040	Br	Bromine	52.000	—	52.000	1.582
36	83.8000	Kr	Krypton	85.167	—	—	85.167
37	85.4678	Rb	Rubidium	7.767	—	—	7.767

Table 7-2. (continued).

Atomic Number	Atomic Weight	Symbol	Element Name	ATR Beryllium (ppm by wt)	MFC (ppm by wt)	KBI Data (ppm by wt)	Brush Wellman (ppm by wt)
38	87.6200	Sr	Strontium	6.000	—	—	6.000
39	88.9059	Y	Yttrium	1.000	—	—	1.000
40	91.2240	Zr	Zirconium	38.214	—	—	38.214
41	92.9064	Nb	Niobium	11.700	11.7	—	<25.000
42	95.9400	Mo	Molybdenum	10.000	—	<10.000	<17.000
43	98.9062	Tc	Technetium	—	—	—	—
44	101.0700	Ru	Ruthenium	5.000	—	—	5.000
45	102.9055	Rh	Rhodium	0.994	—	—	0.994
46	106.4200	Pd	Palladium	5.000	—	—	5.000
47	107.8682	Ag	Silver	2.167	—	2.167	<3.000
48	112.4110	Cd	Cadmium	1.000	—	<1.000	<2.000
49	114.8200	In	Indium	0.069	—	—	0.069
50	118.7100	Sn	Tin	3.000	—	—	3.000
51	121.7500	Sb	Antimony	0.241	—	—	0.241
52	127.6000	Te	Tellurium	47.467	—	—	47.467
53	126.9045	I	Iodine	10.000	—	<10.000	<10.000
54	131.2900	Xe	Xenon	537.333	—	—	537.333
55	132.9054	Cs	Cesium	0.201	—	—	0.201
56	137.3270	Ba	Barium	6.000	—	—	6.000
57	138.9055	La	Lanthanum	1.000	—	<1.000	<3.000
58	140.1150	Ce	Cerium	1.000	—	<1.000	<1.000
59	140.9077	Pr	Praseodymium	1.000	—	<1.000	<0.500
60	144.2400	Nd	Neodymium	5.000	—	<5.000	<0.500
61	—	Pm	Promethium	—	—	—	—
62	150.3600	Sm	Samarium	0.500	—	<0.500	<0.500
63	151.9650	Eu	Europium	0.500	—	<0.500	<0.500
64	157.2500	Gd	Gadolinium	0.200	—	<0.200	<0.500
65	158.9253	Tb	Terbium	1.000	—	<1.000	<1.000
66	162.5000	Dy	Dysprosium	0.200	—	<0.200	<0.500
67	164.9303	Ho	Holmium	1.000	—	<1.000	<0.500
68	167.2600	Er	Erbium	0.500	—	<0.500	<0.500
69	168.9342	Tm	Thulium	0.500	—	<0.500	<0.500
70	173.0400	Yb	Ytterbium	0.200	—	<0.200	<1.000
71	174.9670	Lu	Lutetium	0.667	—	<0.667	<1.000
72	178.4900	Hf	Hafnium	0.423	—	—	0.423
73	180.9479	Ta	Tantalum	0.433	—	—	0.433
74	183.8500	W	Tungsten	76.214	—	—	<76.214
75	186.2070	Re	Rhenium	0.644	—	—	<0.644
76	190.2000	Os	Osmium	0.637	—	—	<0.637
77	192.2200	Ir	Iridium	0.005	—	—	<0.005
78	195.0800	Pt	Platinum	101.867	—	—	<101.867

Table 7-2. (continued).

Atomic Number	Atomic Weight	Symbol	Element Name	ATR Beryllium (ppm by wt)	MFC (ppm by wt)	KBI Data (ppm by wt)	Brush Wellman (ppm by wt)
79	196.9665	Au	Gold	24.800	—	—	24.800
80	200.5900	Hg	Mercury	4.073	—	—	<4.073
81	204.3833	Tl	Thallium	25.000	—	—	<25.000
82	207.2000	Pb	Lead	1.000	—	<1.000	<20.000
83	208.9804	Bi	Bismuth	—	—	—	<5.000
84	—	Po	Polonium	—	—	—	—
85	—	At	Astatine	—	—	—	—
86	—	Rn	Radon	—	—	—	—
87	—	Fr	Francium	—	—	—	—
88	—	Ra	Radium	—	—	—	—
89	—	Ac	Actinium	—	—	—	—
90	232.0381	Th	Thorium	0.438	—	—	<0.438
91	—	Pa	Protactinium	—	—	—	—
92	238.0289	U	Uranium	30.000	30.000	—	71.503

ATR = Advanced Test Reactor

KBI = Kawecki Berylco Industries

MFC = Materials and Fuels Complex

Best-estimate data for elemental concentrations in beryllium metal (see Tables 7-2 and 7-3) are slightly different than those previously reported by Gay (Logan 1999). These differences are due to previous results being applied to beryllium metal obtained from Brush Wellman, while current best-estimated data are based on KBI beryllium metal. Some of the measured data from MFC were not available for the Gay report (Logan 1999).

One important assumption in the computer code analysis is that elemental concentrations are uniformly distributed throughout each reflector block or OSCC (before irradiation). Though no specific information from KBI affirms this, some supporting data from Brush Wellman on nitrogen data support this assumption. Information from Brush Wellman for S-65C grade beryllium indicates that nitrogen concentration is evenly distributed throughout the pressed billets. Because there does not appear to be any physical reason for the existence of large concentration gradients within manufactured billets, all elemental impurities are assumed to be uniformly distributed throughout each beryllium component (before irradiation). After irradiation, newly generated isotopes (and depletion of parent isotopes) will produce different concentrations throughout the irradiated block. Therefore, the first set of collected test samples was obtained from regions of each reflector block (e.g., Site 1) that minimized the effects of neutron irradiation, allowing for an accurate determination of its beginning-of-life conditions.

Table 7-3. Best-estimate elemental composition of beryllium from Kawecki Berylco Industries.

Element Symbol	Element Name	Number	Atomic Weight	KBI Beryllium Concentration (ppm by wt)	Input Mass for a 81,420-g Block Mass (g)	Input Mass for a 54,431-g OSCC Mass (g)
H	Hydrogen	1	1.0079	—	—	—
He	Helium	2	4.0026	—	—	—
Li	Lithium	3	6.9410	1.000	0.081	0.054
Be	Beryllium	4	9.0122	980,667.835	79,845.975	53,378.731

Table 7-3. (continued).

Element Symbol	Element Name	Number	Atomic Weight	KBI Beryllium Concentration (ppm by wt)	Input Mass for a 81,420-g Block Mass (g)	Input Mass for a 54,431-g OSCC Mass (g)
B	Boron	5	10.8110	1.917	0.156	0.104
C	Carbon	6	12.0110	745.000	60.658	40.551
N	Nitrogen	7	14.0067	205.400	16.724	11.180
O	Oxygen	8	15.9994	12,618.667	1,027.412	686.847
F	Fluorine	9	18.9984	69.167	5.632	3.765
Ne	Neon	10	20.1797	1,425.000	116.024	77.564
Na	Sodium	11	22.9898	0.874	0.071	0.048
Mg	Magnesium	12	24.3050	45.000	3.664	2.449
Al	Aluminum	13	26.9815	355.833	28.972	19.368
Si	Silicon	14	28.0855	364.167	29.650	19.822
P	Phosphorus	15	30.9738	50.000	4.071	2.722
S	Sulfur	16	32.0660	7.500	0.611	0.408
Cl	Chlorine	17	35.4527	50.000	4.071	2.722
Ar	Argon	18	39.9480	6.370	0.519	0.347
K	Potassium	19	39.0983	13.070	1.064	0.711
Ca	Calcium	20	40.0780	200.000	16.284	10.886
Sc	Scandium	21	44.9559	2.300	0.187	0.125
Ti	Titanium	22	47.8800	61.667	5.021	3.357
V	Vanadium	23	50.9415	3.423	0.279	0.186
Cr	Chromium	24	51.9961	92.500	7.531	5.035
Mn	Manganese	25	54.9381	56.667	4.614	3.084
Fe	Iron	26	55.8470	1,499.167	122.062	81.601
Co	Cobalt	27	58.9332	12.000	0.977	0.653
Ni	Nickel	28	58.6900	225.833	18.387	12.292
Cu	Copper	29	63.5460	87.500	7.124	4.763
Zn	Zinc	30	65.3900	13.000	1.058	0.708
Ga	Gallium	31	69.7230	0.859	0.070	0.047
Ge	Germanium	32	72.6100	5.000	0.407	0.272
As	Arsenic	33	74.9216	1.782	0.145	0.097
Se	Selenium	34	78.9600	2.383	0.194	0.130
Br	Bromine	35	79.9040	52.000	4.234	2.830
Kr	Krypton	36	83.8000	85.167	6.934	4.636
Rb	Rubidium	37	85.4678	7.767	0.632	0.423
Sr	Strontium	38	87.6200	6.000	0.489	0.327
Y	Yttrium	39	88.9059	1.000	0.081	0.054
Zr	Zirconium	40	91.2240	38.214	3.111	2.080
Nb	Niobium	41	92.9064	11.700	0.953	0.637
Mo	Molybdenum	42	95.9400	10.000	0.814	0.544
Tc	Technetium	43	98.9062	—	—	—
Ru	Ruthenium	44	101.0700	5.000	0.407	0.272
Rh	Rhodium	45	102.9055	0.994	0.081	0.054



Table 7-3. (continued).

Element Symbol	Element Name	Number	Atomic Weight	KBI Beryllium Concentration (ppm by wt)	Input Mass for a 81,420-g Block Mass (g)	Input Mass for a 54,431-g OSCC Mass (g)
Pd	Palladium	46	106.4200	5.000	0.407	0.272
Ag	Silver	47	107.8682	2.167	.176	0.118
Cd	Cadmium	48	112.4110	1.000	0.081	0.054
In	Indium	49	114.8200	0.069	0.006	0.004
Sn	Tin	50	118.7100	3.000	0.244	0.163
Sb	Antimony	51	121.7500	0.241	0.020	0.013
Te	Tellurium	52	127.6000	47.467	3.865	2.584
I	Iodine	53	126.9045	10.000	0.814	0.544
Xe	Xenon	54	131.2900	537.333	43.750	29.248
Cs	Cesium	55	132.9054	0.201	0.016	0.011
Ba	Barium	56	137.3270	6.000	0.489	0.327
La	Lanthanum	57	138.9055	1.000	0.081	0.054
Ce	Cerium	58	140.1150	1.000	0.081	0.054
Pr	Praseodymium	59	140.9077	1.000	0.081	0.054
Nd	Neodymium	60	144.2400	5.000	0.407	0.272
Pm	Promethium	61	144.9145	—	—	—
Sm	Samarium	62	150.3600	0.500	0.041	0.027
Eu	Europium	63	151.9650	0.500	0.041	0.027
Gd	Gadolinium	64	157.2500	0.200	0.016	0.011
Tb	Terbium	65	158.9253	1.000	0.081	0.054
Dy	Dysprosium	66	162.5000	0.200	0.016	0.011
Ho	Holmium	67	164.9303	1.000	0.081	0.054
Er	Erbium	68	167.2600	0.500	0.041	0.027
Tm	Thulium	69	168.9342	0.500	0.041	0.027
Yb	Ytterbium	70	173.0400	0.200	0.016	0.011
Lu	Lutetium	71	174.9670	0.667	0.054	0.036
Hf	Hafnium	72	178.4900	0.423	0.034	0.023
Ta	Tantalum	73	180.9479	0.433	0.035	0.024
W	Tungsten	74	183.8500	76.214	6.205	4.148
Re	Rhenium	75	186.2070	0.644	0.052	0.035
Os	Osmium	76	190.2000	0.637	0.052	0.035
Ir	Iridium	77	192.2200	0.005	—	—
Pt	Platinum	78	195.0800	101.867	8.294	5.545
Au	Gold	79	196.9665	24.800	2.019	1.350
Hg	Mercury	80	200.5900	4.073	0.332	0.222
Tl	Thallium	81	204.3833	25.000	2.036	1.361
Pb	Lead	82	207.2000	1.000	0.081	0.054
Bi	Bismuth	83	208.9804	—	—	—
Po	Polonium	84	—	—	—	—
At	Astatine	85	—	—	—	—
Rn	Radon	86	—	—	—	—

Table 7-3. (continued).

Element Symbol	Element Name	Number	Atomic Weight	KBI Beryllium Concentration (ppm by wt)	Input Mass for a 81,420-g Block Mass (g)	Input Mass for a 54,431-g OSCC Mass (g)
Fr	Francium	87	—	—	—	—
Ra	Radium	88	—	—	—	—
Ac	Actinium	89	—	—	—	—
Th	Thorium	90	232.0381	0.438	0.036	0.024
Pa	Protactinium	91	—	—	—	—
U	Uranium	92	238.0289	30.000	2.443	1.633
			Totals	1,000,000.000	81,420.000	54,431.000

KBI = Kawecki Berylco Industries  
OSCC = outer shim control cylinder

## 7.4 Physical Descriptions of Reflector Blocks and Outer Shim Control Cylinders from the Advanced Test Reactor

Figure 6-1 shows a schematic of a right-side reflector block, 010R, in a vertical orientation. Figure 7-4 shows a horizontal cross section of a left-side reflector block with some important dimensions. Figure 7-5 shows a schematic of two attached ATR reflector blocks; note that the top side of both blocks is shown on the right side of this figure. In Figure 7-4, the right block is identified as Part 419609-1 and the left block is shown as Part 419609-2. The average weight of the beryllium metal contained in each reflector block (i.e., without its associated nonberyllium hardware) is approximately 81,420 g (179.5 lb). The density of beryllium metal is 1.85 g/cm<sup>3</sup>. Therefore, the metal volume of a reflector block is approximately 44,000 cm<sup>3</sup> (0.044 m<sup>3</sup>). The height of each block is 130 cm (51 in.) and the active ATR core height is 122 cm (48 in.). Thus portions of each reflector block extend above the reactor fuel. The cross-sectional (metal) area of an ATR reflector block is approximately 340 cm<sup>2</sup> (53 in.<sup>2</sup>).

The weight of a single ATR reflector block without the nonberyllium hardware has been measured by Speedring (currently known as Axsys Technologies, Cullman, Alabama, the company that currently machines the ATR beryllium blocks) to be 81,420 g (179.5 lb). This weight represents a current block design; that is, one with saw cuts. Blocks without saw cuts are estimated to weigh about 81,650 g (180 lb). To simplify the computer modeling details (especially the input mass of elements that define the composition of a block), and have one model apply to both types of reflector block configurations, all ATR reflector blocks (both with and without saw cuts) were assumed to have a beryllium weight of 81,420 g (179.5 lb).

The estimated beryllium weight of an OSCC is 54,400 g (120 lb) and its corresponding metal volume is about 30,000 cm<sup>3</sup>. All new OSCCs, and most of the older OSCCs, were constructed of three separate axial sections of beryllium components (as illustrated in Figures 7-6 and 7-7).

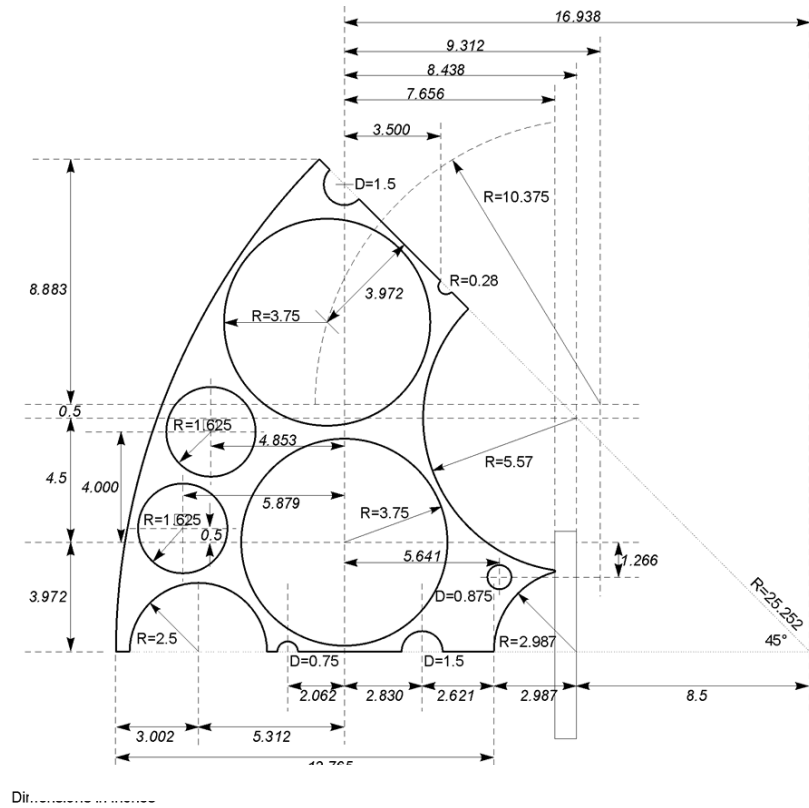


Figure 7-4. Horizontal cross section showing dimensional data of a beryllium reflector block from the Advanced Test Reactor. The illustrated block represents the left side of a block, assuming that the top surface is visible.

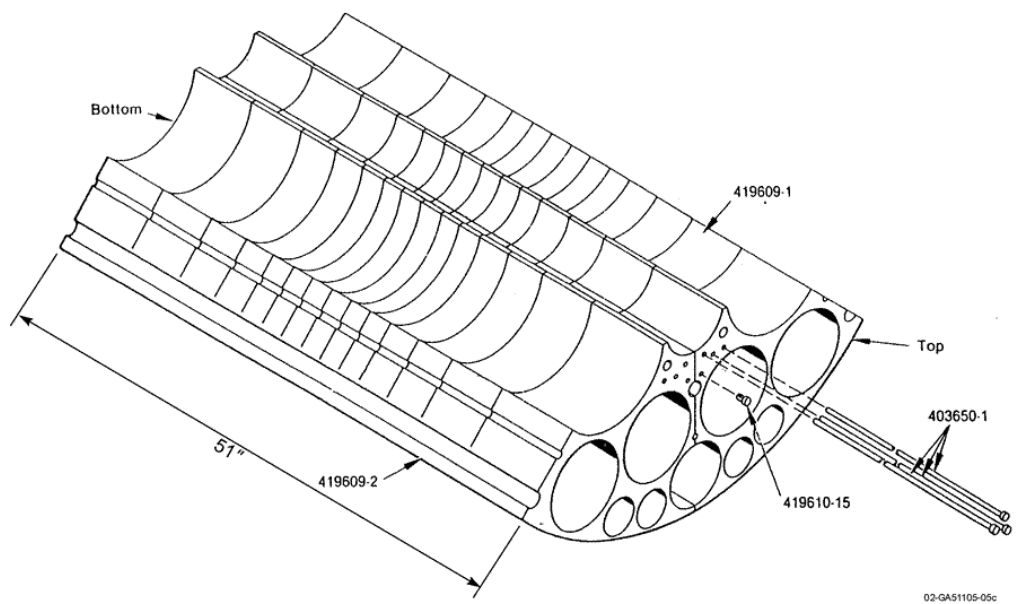


Figure 7-5. Two beryllium reflector blocks from the Advanced Test Reactor positioned together to form one single reflector lobe.

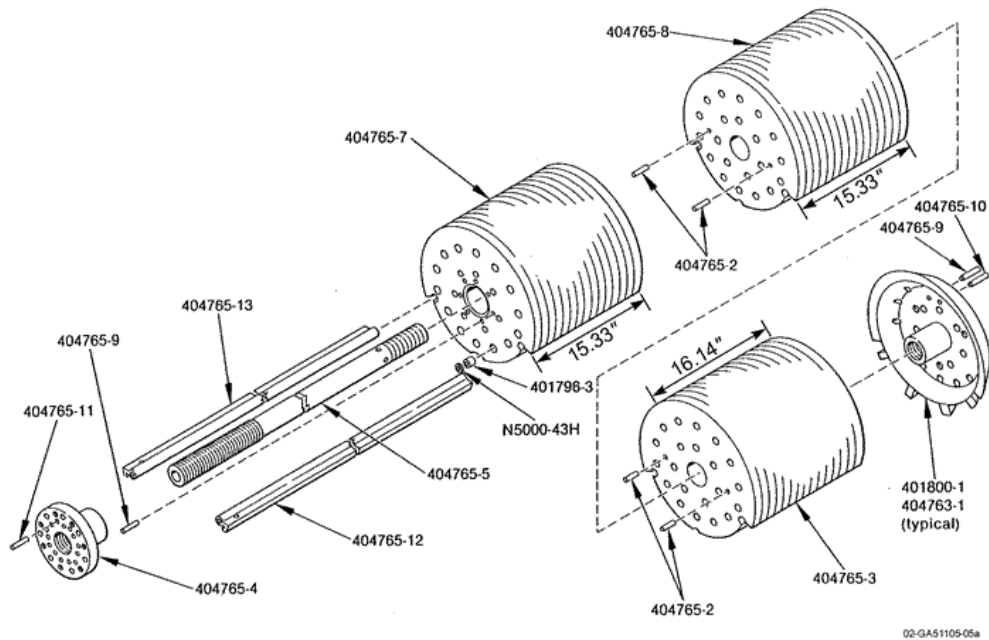


Figure 7-6. A schematic of a disassembled outer shim control cylinder showing its key components.

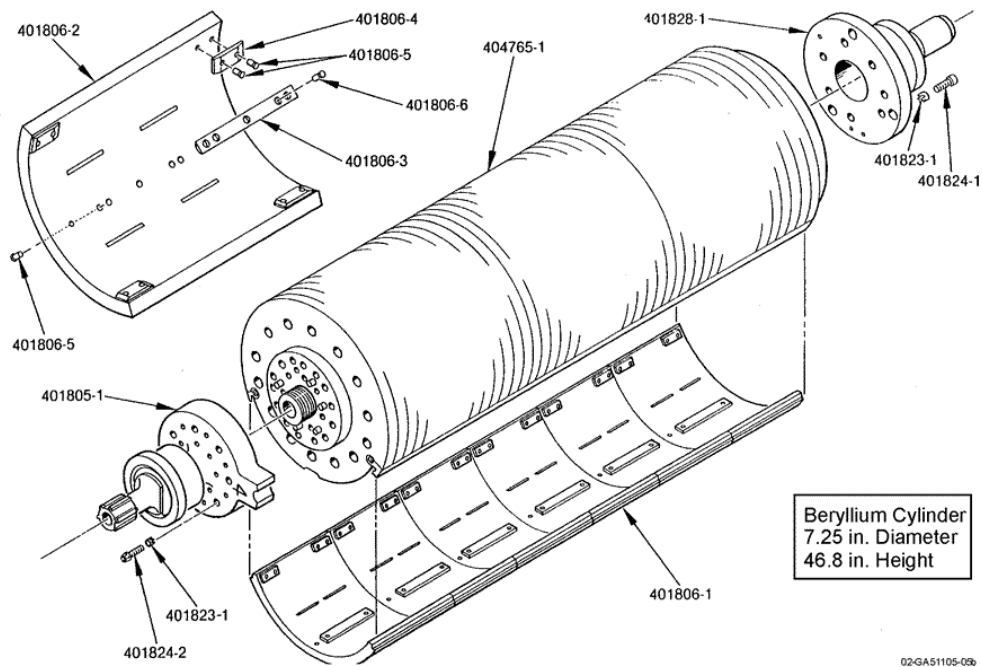


Figure 7-7. An outer shim control cylinder that is partially assembled.

The height of each beryllium segment varied from approximately 39 cm (15.33 in.) for the upper and center sections to 41 cm (16.14 in.) for the lower segment. Total height of the three beryllium sections is 119 cm (46.8 in.). Because of its component construction, each beryllium section within an OSCC has a good chance of being made from different beryllium pressings (or billets), and each section can have different chemical impurities. However, the chemical impurity data are not known for each component of each OSCC. The best-estimate composition of ATR's OSCCs was assumed to be the same as that used for beryllium blocks from ATR. In addition, these concentrations are assumed to apply uniformly to all three sections of each OSCC.

## **7.5 Cross-Sectional Data Used in the Analysis by Oak Ridge Isotope GENERation and Depletion Code Version 2**

For the ORIGEN2 calculations, one-group neutron cross-section libraries were constructed from several different data sets. First, the INL standard ATR cross-section library was applied to all ORIGEN2 calculations and each radionuclide that was not otherwise explicitly modeled with a substitution data set. The substitution library was produced from MCNP4B calculations for those radionuclides: Li-6, Be-9, C-12, C-13, N-14, O-17, Co-59, Co-60, Co-61, Ni-58, Ni-59, Ni-60, Ni-61, Ni-62, Ni-63, Ni-64, Cu-63, Zn-66, Nb-93, Nb-94, Mo-94, Mo-98, Mo-99, Tc-99, Th-232, Th-233, Pa-233, U-233, U-234, U-235, U-236, U-237, U-238, U-239, U-240, Np-235, Np-236, Np-237, Np-238, Pu-237, Pu-238, Pu-239, Pu-240, Pu-241, Pu-242, Pu-243, Am-241, Am-242, Am-243, Cm-242, Cm-243, Cm-244, Cm-245, Cm-246, Cm-247, Cm-248, Bk-249, Cf-249, Cf-250, Cf-251, and Cf-252. Four explicit cross-section data sets were generated. One library was generated for the Site 1 (low-flux) region of Block 010R, one set was generated for the Site 2 (high-flux) region of Block 010R, and another set was produced for the average region of Block 010R. A fourth set was generated for an OSCC.

Cross sections for Sites 1 and 2 were then used in the ORIGEN2 calculations that modeled these specific locations. Calculations for Sites 1 and 2 were then compared against measured data collected from these locations. The measured data provided some validation information, and allowed for an estimate of the accuracy of the computer model to reproduce the measured data, thereby providing a measure of the accuracy of the code to determine the total inventories of radionuclides for reflector blocks and OSCCs that were not independently measured. The block average cross-section data set was used in the ORIGEN2 calculations for Block 010R and all other reflector blocks. A separate cross-section data set was generated for the OSCCs.

## **7.6 Oak Ridge Isotope GENERation and Depletion Code Version 2 Model for the Reflector Blocks from the Advanced Test Reactor**

In addition to computer models to determine the entire block inventories from Cores 1, 2, and 3, two specific node calculations were made for Sites 1 and 2 for Block 010R (see Figure 6-1). The purpose of individual node calculations was to assess the ORIGEN2 model against measured data values obtained from these two sample locations. Comparisons of measured data obtained from Site 1 and ORIGEN2 calculated results are shown in Table 7-4. Two samples collected from Site 2 (Samples 82553 and 82919) were analyzed at MFC. Comparisons of measured data against results calculated by computer code are shown in Table 7-5 (for Sample 82553) and Table 7-6 (for Sample 82919). Note that measured TRU inventories at Site 2 are slightly higher than the code results.

Table 7-4. Comparison of measured Sample 79778 and results for Site 1 from Oak Ridge Isotope GENERation and Depletion Code Version 2 using the best-estimate cross sections for Block 010R (Core 3, northeast lobe).

Isotopes	Sample 79778		ORIGEN2 ( $\mu\text{Ci/g}$ )	ORIGEN2 ( $\mu\text{g/g}$ )	Ratio Measured/ ORIGEN2	Comments
	Measured ( $\mu\text{Ci/g}$ )	Measured ( $\mu\text{g/g}$ )				
H-3	200.0	—	341.7	—	0.585	
C-14	0.61	—	1.07	—	0.570	N impurity = 203 ppm = measured data for 79778
Co-60	13.1	—	13.11	—	0.999	Estimated beginning of life Co impurity = 9 ppm
Cs-137	0.20	—	0.22	—	0.918	
Nb-93	—	1	—	1.00	0.998	Beginning of life Nb-93 impurity = 1 ppm
Total U (end of life)	—	30 to 37	—	29.9	1.003 to 1.24	Estimated beginning of life naturally enriched U = 30 ppm
		Ratio		Ratio		
U-235/U-238	—	0.0053	—	0.0047	1.123	Natural ratio = 0.0072
Transuranic Isotopes	Measured (nCi/g)	Measured (ng/g)	ORIGEN2 (nCi/g)	ORIGEN2 (ng/g)	Ratio Measured/ ORIGEN2	Comments
Np-237	—	—	0.000	0.049	—	Half-life = 2,140,000 years
Pu-238	—	—	0.096	0.006	—	Half-life = 87.7 years
Pu-239	4.35	70	5.119	82.31	0.850	Half-life = 24,100 years
Pu-240	—	—	2.051	8.998	—	Half-life = 6,560 years
Pu-241	Not included	—	Not included	—	—	Half-life = 14.4 years
Pu-242	—	—	0.000	0.042	—	Half-life = 376,300 years
Pu-244	—	—	0.000	0.000	—	Half-life = 82,600,000 years, alpha decay = 99.9%
Am-241	—	—	1.296	0.377	—	Half-life = 433 years
Am-243	—	—	0.000	0.000	—	Half-life = 7,370 years
Cm-243	—	—	0.000	0.000	—	Half-life = 29 years, alpha decay = 99.76%
Cm-244	Not included	—	Not included	—	—	Half-life = 18.1 years
Cm-245	—	—	0.000	0.000	—	Half-life = 8,500 years
Cm-246	—	—	0.000	0.000	—	Half-life = 4,760 years
Cm-247	—	—	0.000	0.000	—	Half-life = 15,600,000 years
Cm-248	—	—	0.000	0.000	—	Half-life = 340,000 years, alpha decay = 92%
Total Transuranic Isotopes	4.35	—	8.56	—	0.51	

ORIGEN2 = Oak Ridge Isotope GENERation and Depletion Code Version 2

Transuranic isotopes with a half-life less than 20 years are not included in the determination of transuranic waste.

Note: Flux = 3.466E12 n/cm<sup>2</sup>/second.

Table 7-5. Comparison of measured Sample 82553 and results for Site 2 from Oak Ridge Isotope GENERation and Depletion Code Version 2 using the best-estimate cross sections for Block 010R (Core 3, northeast lobe).

Isotopes	Sample 82553		Site 2		Ratio Measured/ ORIGEN2	Comments
	Measured ( $\mu\text{Ci/g}$ )	Measured ( $\mu\text{g/g}$ )	ORIGEN2 ( $\mu\text{Ci/g}$ )	ORIGEN2 ( $\mu\text{g/g}$ )		
H-3	Not measured	Not measured	1,650,000	—	—	
C-14	Not measured	Not measured	66	—	—	N impurity = 203 ppm = measured data
Co-60	375	—	529	—	0.71	Estimated beginning of life Co impurity = 9 ppm
Cs-137	50	—	55	—	0.91	
Total U (end of life)	—	10.3	—	6.42	1.60	Estimated beginning of life naturally enriched U = 30 ppm
U-235/U-238	—	Ratio <0.00019	—	Ratio 0.00020	<0.95	Natural ratio = 0.0072
Transuranic Isotopes	Measured (nCi/g)	Measured ( $\mu\text{g/g}$ )	ORIGEN2 (nCi/g)	ORIGEN2 ( $\mu\text{g/g}$ )	Ratio Measured/ ORIGEN2	Comments
Np-237	—	—	0.002	0.0022	—	Half-life = 2,140,000 years
Pu-238	34.3	0.002	46.66	0.0027	0.74	Half-life = 87.7 years
Pu-239	14.9	0.240	11.71	0.1882	1.27	Half-life = 24,100 years
Pu-240	52.2	0.230	56.55	0.2481	0.93	Half-life = 6,560 years
Pu-241	Not included	0.020	Not included	0.0266	0.75	Half-life = 14.4 years
Pu-242	0.6	0.150	0.742	0.1942	0.79	Half-life = 376,300 years
Pu-244	—	—	—	—	—	Half-life = 82,600,000 years, alpha decay = 99.9%
Am-241	241	0.070	102.9	0.0300	2.34	Half-life = 433 years
Am-243	41	0.205	12.03	0.0603	3.40	Half-life = 7,370 years
Cm-243	—	—	1.651	0.000032	—	Half-life = 29 years, alpha decay = 99.76%
Cm-244	Not included	0.380	Not included	0.2249	1.69	Half-life = 18.1 years
Cm-245	5.2	0.030	2.985	0.0174	1.73	Half-life = 8,500 years
Cm-246	45.6	0.150	44.270	0.1441	1.04	Half-life = 4,760 years
Cm-247	0.0006	0.007	0.001	0.0080	0.74	Half-life = 15,600,000 years
Cm-248	—	—	0.048	0.0112	—	Half-life = 340,000 years, alpha decay = 92%
Total Transuranic Isotopes	434.8	—	279.5	—	1.56	

ORIGEN2 = Oak Ridge Isotope GENERation and Depletion Code Version 2

Transuranic isotopes with a half-life less than 20 years are not included in the determination of transuranic waste.

Note: Flux =  $6.704\text{E}14$  n/cm<sup>2</sup>/second.

Table 7-6. Comparison of measured Sample 82919 and results for Site 2 from Oak Ridge Isotope GENERation and Depletion Code Version 2 using the best-estimate cross sections for Block 010R (Core 3, northeast lobe).

Isotopes	Sample 82919		Site 2		Ratio Measured/ ORIGEN2	Comments
	Measured ( $\mu\text{Ci/g}$ )	Measured ( $\mu\text{g/g}$ )	ORIGEN2 ( $\mu\text{Ci/g}$ )	ORIGEN2 ( $\mu\text{g/g}$ )		
H-3	840,000	—	1,650,000	—	0.509	
C-14	41	—	66	—	0.621	N impurity = 203 ppm = measured data
Co-60	380	—	529	—	0.718	Estimated beginning of life Co impurity = 9 ppm
Cs-137	51	—	55	—	0.927	
Total U (end of life)	—	8.71	—	6.42	1.35	Estimated beginning of life naturally enriched U = 30 ppm
U-235/U-238	—	Ratio 0.0081	—	Ratio 0.00020	See comment	Natural ratio = 0.0072 Probable error in the measured Materials and Fuels Complex result for U-235
Transuranic Isotopes	Measured (nCi/g)	Measured ( $\mu\text{g/g}$ )	ORIGEN2 (nCi/g)	ORIGEN2 ( $\mu\text{g/g}$ )	Ratio Measured/ ORIGEN2	Comments
Np-237	—	— < 0.01	0.002	0.0022	—	Half-life = 2,140,000 years
Pu-238	61.56	0.0036	46.66	0.0027	1.32	Half-life = 87.7 years
Pu-239	13.0	0.210	11.71	0.1882	1.11	Half-life = 24,100 years
Pu-240	63.6	0.280	56.55	0.2481	1.13	Half-life = 6,560 years
Pu-241	Not included	0.020	Not included	0.0266	0.75	Half-life = 14.4 years
Pu-242	0.79	0.20	0.742	0.1942	1.06	Half-life = 376,300 years
Pu-244	—	—	—	—	—	Half-life = 82,600,000 years, alpha decay = 99.9%
Am-241	310	0.09	102.9	0.0300	3.0	Half-life = 433 years
Am-243	48	0.24	12.03	0.0603	4.0	Half-life = 7,370 years
Cm-243	—	—	1.651	0.000032	—	Half-life = 29 years, alpha decay = 99.76%
Cm-244	Not included	0.25	Not included	0.2249	1.11	Half-life = 18.1 years
Cm-245	3.4	0.02	2.985	0.0174	1.14	Half-life = 8,500 years
Cm-246	33.4	0.11	44.27	0.1441	0.97	Half-life = 4,760 years
Cm-247	0	0	0.001	0.0080	0	Half-life = 15,600,000 years
Cm-248	—	—	0.048	0.0112	—	Half-life = 340,000 years, alpha decay = 92%
Total Transuranic Isotopes	533.4	—	279.5	—	1.91	

ORIGEN2 = Oak Ridge Isotope GENERation and Depletion Code Version 2

Transuranic isotopes with half-life less than 20 years are not included in the determination of transuranic waste.

Note: Flux = 6.704E14 n/cm<sup>2</sup>/second.



The ORIGEN2 model for reflector blocks from ATR's Core 1 considered one block from each of the four lobes. Because all eight blocks from Core 1 were disposed of and the alternate blocks from each lobe would have an inventory equal to that calculated in the ORIGEN2 model, the entire inventory from Core 1 can be determined by multiplying the ORIGEN2 results by a factor of 2.

## **7.7 Oak Ridge Isotope Generation and Depletion Code Version 2 Model for the Outer Shim Control Cylinders from the Advanced Test Reactor**

Only nine OSCCs have been disposed of and all of these shim cylinders have come from Core 2. Note that OSCCs in Core 2 also saw irradiation in Core 1. That is, the shim cylinders were used in both Cores 1 and 2. Because it is not known which nine of the 16 OSCCs were disposed of, the computer code model calculated the total inventory for all 16 OSCCs. The inventory for those OSCCs that were disposed of in the SDA can be determined by multiplying the total OSCC inventory by 9/16 (0.5625).

## **7.8 Results of Best-Estimate Calculated Inventory of Reflector Blocks and Outer Shim Control Cylinders from the Advanced Test Reactor**

Tables 7-7 through 7-16 show inventories of beryllium components from ATR disposed of in the SDA that were calculated using ORIGEN2. Results for ATR's reflector blocks are given in Tables 7-7 through 7-12, and the corresponding results for ATR's OSCCs are shown in Tables 7-13 and 7-14. Though the ORIGEN2 code can calculate the production and decay of several hundred radionuclides (e.g., 688 activation products, 129 actinides + daughters, and 879 fission products), only the results of the 44 most important radionuclides are listed in these tables.

The table values are separated into four major groups (the blocks from Cores 1, 2, and 3; and the OSCCs from Cores 1 and 2). All results are computed for two different decay times (the specific disposal date and a common decay date of September 15, 2001). For example, the calculated inventory for the eight reflector blocks disposed of from Core 1 is shown in Table 7-7 for the disposal date of December 1, 1976, and Table 7-8 for the common decay date of September 15, 2001. The curie results shown in Columns 3, 4, 5, and 6 of Table 7-7 represent the calculated block inventories for one block located in the NW lobe of Core 1, one block from the NE lobe, one block from the SW lobe, and one block from the SE lobe. Each lobe position contains two blocks and all eight blocks were disposed of from Core 1, the total block inventory from Core 1 (e.g., the Column 7 data) can be computed as follows: the total inventory for the eight blocks disposed of from Core 1 (Column 7) equals  $2 \times$  NW lobe inventory (Column 3) +  $2 \times$  NE lobe inventory (Column 4) +  $2 \times$  SW lobe inventory (Column 5) +  $2 \times$  SE lobe inventory (Column 6). At the bottom of these tables, the TRU concentration (nano-curies per gram) is calculated for those TRU isotopes with half-lives greater than 20 years. The total lobe megawatt-day energy generation, the total beryllium mass, and metal volume for each beryllium component also are shown at the bottom of each table.

As an example, consider Block 011R from Core 3 (see Column 6 of Table 7-11). From Figure 7-3, or Table 7-1, Block 011R was one of the six blocks disposed of from Core 3. Only Blocks 010R and 016L from Core 3 remain in the ATR canal. From Table 7-11, the ORIGEN2-calculated inventory for C-14 is listed as 2.50 Ci. The Pu-239 inventory for Block 011R is shown as 1.91E-03 Ci. The average TRU concentration for Block 011R is shown as 341 nCi/g, and the average TRU concentration for all six blocks is listed in Table 7-11 as 377 nCi/g. All of these results were computed relative to the estimated disposal date of July 1, 1993. Similar results computed for the common decay date of September 15, 2001, for Core 3 are shown in Table 7-12.

Table 7-7. Inventory calculated using Oak Ridge Isotope Generation and Depletion Code Version 2 at the estimated disposal date of December 1, 1976, for the Advanced Test Reactor beryllium blocks located in Core 1.

Isotope	Half-life (years)	Lobe NW	Lobe NE	Lobe SW	Lobe SE	Total Inventory for Eight Blocks (Ci for eight blocks)
		NW-L or NW-R (Ci per block)	NE-L or NE-R (Ci per block)	SW-L or SW-R (Ci per block)	SE-L or SE-R (Ci per block)	
H-3	1.23E+01	1.68E+04	1.61E+04	1.62E+04	1.62E+04	1.31E+05
Be-10	1.60E+06	1.25E-01	1.21E-01	1.21E-01	1.21E-01	9.76E-01
C-14	5.73E+03	1.00E+00	9.68E-01	9.68E-01	9.70E-01	7.81E+00
Cl-36	3.01E+05	8.39E-03	8.13E-03	8.14E-03	8.15E-03	6.56E-02
Co-60	5.27E+00	9.89E+01	9.62E+01	9.62E+01	9.63E+01	7.75E+02
Ni-59	7.60E+04	2.10E-02	2.05E-02	2.05E-02	2.06E-02	1.65E-01
Ni-63	1.00E+02	3.74E+00	3.64E+00	3.64E+00	3.64E+00	2.93E+01
Sr-90	2.91E+01	3.22E-01	3.12E-01	3.12E-01	3.13E-01	2.52E+00
Nb-94	2.00E+04	2.25E-03	2.19E-03	2.19E-03	2.19E-03	1.76E-02
Tc-99	2.13E+05	1.30E-04	1.26E-04	1.26E-04	1.26E-04	1.02E-03
I-129	1.57E+07	9.52E-07	9.22E-07	9.22E-07	9.23E-07	7.44E-06
Cs-137	3.02E+01	1.04E+00	1.01E+00	1.01E+00	1.00E+00	8.12E+00
Eu-152	1.35E+01	2.87E-02	3.28E-02	3.27E-02	3.26E-02	2.54E-01
Eu-154	8.59E+00	1.89E+00	1.91E+00	1.91E+00	1.91E+00	1.52E+01
Pb-210	2.23E+01	2.31E-12	2.13E-12	2.13E-12	2.14E-12	1.74E-11
Ra-226	1.60E+03	7.25E-13	7.09E-13	7.09E-13	7.10E-13	5.71E-12
Ra-228	5.76E+00	2.13E-09	2.13E-09	2.13E-09	2.13E-09	1.70E-08
Ac-227	2.18E+01	5.34E-09	5.28E-09	5.28E-09	5.28E-09	4.24E-08
Th-228	1.91E+00	8.57E-06	8.20E-06	8.21E-06	8.22E-06	6.64E-05
Th-229	7.30E+03	4.98E-09	4.97E-09	4.97E-09	4.97E-09	3.98E-08
Th-230	7.54E+04	3.04E-10	2.98E-10	2.98E-10	2.98E-10	2.40E-09
Th-232	1.40E+10	3.53E-09	3.54E-09	3.54E-09	3.54E-09	2.83E-08
Pa-231	3.28E+04	2.96E-08	2.92E-08	2.93E-08	2.93E-08	2.35E-07
U-232	7.00E+01	9.72E-06	9.31E-06	9.31E-06	9.33E-06	7.53E-05
U-233	1.59E+05	7.74E-06	7.73E-06	7.73E-06	7.73E-06	6.19E-05
U-234	2.46E+05	1.72E-06	1.68E-06	1.69E-06	1.69E-06	1.36E-05
U-235	7.04E+08	4.26E-10	4.74E-10	4.73E-10	4.71E-10	3.69E-09
U-236	2.34E+07	1.46E-07	1.47E-07	1.47E-07	1.47E-07	1.17E-06
U-238	4.47E+09	6.80E-07	6.84E-07	6.84E-07	6.84E-07	5.46E-06
Np-237	2.14E+06	1.98E-07	1.96E-07	1.96E-07	1.96E-07	1.57E-06
Pu-238	8.77E+01	1.06E-02	1.05E-02	1.05E-02	1.05E-02	8.42E-02
Pu-239	2.41E+04	2.51E-03	2.52E-03	2.52E-03	2.52E-03	2.01E-02
Pu-240	6.56E+03	4.14E-03	4.15E-03	4.15E-03	4.15E-03	3.32E-02
Pu-241	1.44E+01	9.00E-01	9.02E-01	9.02E-01	9.02E-01	7.21E+00
Pu-242	3.75E+05	6.34E-05	6.12E-05	6.12E-05	6.13E-05	4.94E-04
Pu-244	8.00E+07	4.38E-11	3.91E-11	3.92E-11	3.93E-11	3.23E-10
Am-241	4.33E+02	8.07E-03	8.12E-03	8.12E-03	8.12E-03	6.49E-02
Am-243	7.37E+03	6.19E-04	5.82E-04	5.83E-04	5.84E-04	4.74E-03

Table 7-7. (continued).

Isotope	Half-life (years)	Lobe NW	Lobe NE	Lobe SW	Lobe SE	Total Inventory for Eight Blocks (Ci for eight blocks)
		NW-L or NW-R (Ci per block)	NE-L or NE-R (Ci per block)	SW-L or SW-R (Ci per block)	SE-L or SE-R (Ci per block)	
Cm-243	2.91E+01	2.53E-04	2.48E-04	2.48E-04	2.48E-04	2.00E-03
Cm-244	1.81E+01	1.59E-01	1.43E-01	1.44E-01	1.44E-01	1.18E+00
Cm-245	8.50E+03	8.56E-06	7.65E-06	7.66E-06	7.69E-06	6.31E-05
Cm-246	4.76E+03	8.40E-06	7.18E-06	7.19E-06	7.24E-06	6.00E-05
Cm-247	1.56E+07	2.96E-11	2.44E-11	2.45E-11	2.47E-11	2.06E-10
Cm-248	3.48E+05	1.58E-10	1.25E-10	1.26E-10	1.27E-10	1.07E-09
Transuranic concentration (nCi/g) =		323	322	322	322	322
Lobe MWd =		28,894	27,967	27,978	28,017	For 8 blocks
Beryllium mass (g) =		81,420	81,420	81,420	81,420	651,360
Metal volume (m <sup>3</sup> ) =		0.0440	0.0440	0.0440	0.0440	0.3521

NE-L = northeast-left  
NE-R = northeast-right  
NW-L = northwest-left  
NW-R = northwest-right  
SE-L = southeast-left  
SE-R = southeast-right  
SW-L = southwest-left  
SW-R = southwest-right

Table 7-8. Inventory calculated using Oak Ridge Isotope Generation and Depletion Code Version 2 at the decay time of September 15, 2001, for the Advanced Test Reactor beryllium blocks located in Core 1.

Isotope	Half-life (years)	Lobe NW	Lobe NE	Lobe SW	Lobe SE	Total Inventory for Eight Blocks (Ci for eight blocks)
		NW-L or NW-R (Ci per block)	NE-L or NE-R (Ci per block)	SW-L or SW-R (Ci per block)	SE-L or SE-R (Ci per block)	
H-3	1.23E+01	4.17E+03	4.01E+03	4.02E+03	4.02E+03	3.24E+04
Be-10	1.60E+06	1.25E-01	1.21E-01	1.21E-01	1.21E-01	9.76E-01
C-14	5.73E+03	9.97E-01	9.65E-01	9.65E-01	9.67E-01	7.79E+00
Cl-36	3.01E+05	8.39E-03	8.13E-03	8.14E-03	8.15E-03	6.56E-02
Co-60	5.27E+00	3.80E+00	3.69E+00	3.69E+00	3.70E+00	2.98E+01
Ni-59	7.60E+04	2.10E-02	2.05E-02	2.05E-02	2.06E-02	1.65E-01
Ni-63	1.00E+02	3.11E+00	3.02E+00	3.02E+00	3.02E+00	2.43E+01
Sr-90	2.91E+01	1.79E-01	1.73E-01	1.73E-01	1.73E-01	1.40E+00
Nb-94	2.00E+04	2.25E-03	2.19E-03	2.19E-03	2.19E-03	1.76E-02
Tc-99	2.13E+05	1.30E-04	1.26E-04	1.26E-04	1.26E-04	1.02E-03
I-129	1.57E+07	9.52E-07	9.22E-07	9.22E-07	9.23E-07	7.44E-06
Cs-137	3.02E+01	5.89E-01	5.69E-01	5.69E-01	5.70E-01	4.59E+00
Eu-152	1.35E+01	8.10E-03	9.27E-03	9.26E-03	9.20E-03	7.17E-02
Eu-154	8.59E+00	2.56E-01	2.59E-01	2.59E-01	2.59E-01	2.07E+00
Pb-210	2.23E+01	2.93E-12	2.80E-12	2.81E-12	2.81E-12	2.27E-11
Ra-226	1.60E+03	6.30E-12	6.17E-12	6.17E-12	6.18E-12	4.96E-11
Ra-228	5.76E+00	3.42E-09	3.44E-09	3.44E-09	3.43E-09	2.75E-08
Ac-227	2.18E+01	1.86E-08	1.84E-08	1.84E-08	1.84E-08	1.48E-07

Table 7-8. (continued).

Isotope	Half-life (years)	Lobe NW	Lobe NE	Lobe SW	Lobe SE	Total Inventory for Eight Blocks (Ci for eight blocks)
		NW-L or NW-R (Ci per block)	NE-L or NE-R (Ci per block)	SW-L or SW-R (Ci per block)	SE-L or SE-R (Ci per block)	
Th-228	1.91E+00	7.87E-06	7.54E-06	7.54E-06	7.55E-06	6.10E-05
Th-229	7.30E+03	2.31E-08	2.30E-08	2.30E-08	2.30E-08	1.84E-07
Th-230	7.54E+04	7.64E-10	7.50E-10	7.50E-10	7.51E-10	6.03E-09
Th-232	1.40E+10	3.53E-09	3.54E-09	3.54E-09	3.54E-09	2.83E-08
Pa-231	3.28E+04	2.96E-08	2.92E-08	2.92E-08	2.93E-08	2.35E-07
U-232	7.00E+01	7.66E-06	7.33E-06	7.34E-06	7.35E-06	5.94E-05
U-233	1.59E+05	7.74E-06	7.73E-06	7.73E-06	7.73E-06	6.19E-05
U-234	2.46E+05	2.39E-06	2.35E-06	2.35E-06	2.35E-06	1.89E-05
U-235	7.04E+08	4.87E-10	5.36E-10	5.35E-10	5.33E-10	4.18E-09
U-236	2.34E+07	1.49E-07	1.50E-07	1.50E-07	1.50E-07	1.20E-06
U-238	4.47E+09	6.80E-07	6.84E-07	6.84E-07	6.84E-07	5.46E-06
Np-237	2.14E+06	3.61E-07	3.59E-07	3.59E-07	3.59E-07	2.88E-06
Pu-238	8.77E+01	8.68E-03	8.61E-03	8.61E-03	8.61E-03	6.90E-02
Pu-239	2.41E+04	2.51E-03	2.52E-03	2.52E-03	2.52E-03	2.01E-02
Pu-240	6.56E+03	4.40E-03	4.38E-03	4.38E-03	4.38E-03	3.51E-02
Pu-241	1.44E+01	2.73E-01	2.74E-01	2.74E-01	2.73E-01	2.19E+00
Pu-242	3.75E+05	6.34E-05	6.12E-05	6.12E-05	6.13E-05	4.94E-04
Pu-244	8.00E+07	4.38E-11	3.91E-11	3.92E-11	3.93E-11	3.23E-10
Am-241	4.33E+02	2.82E-02	2.83E-02	2.83E-02	2.82E-02	2.26E-01
Am-243	7.37E+03	6.17E-04	5.81E-04	5.81E-04	5.83E-04	4.72E-03
Cm-243	2.91E+01	1.39E-04	1.35E-04	1.36E-04	1.36E-04	1.09E-03
Cm-244	1.81E+01	6.16E-02	5.55E-02	5.56E-02	5.58E-02	4.57E-01
Cm-245	8.50E+03	8.55E-06	7.63E-06	7.64E-06	7.68E-06	6.30E-05
Cm-246	4.76E+03	8.37E-06	7.15E-06	7.16E-06	7.21E-06	5.98E-05
Cm-247	1.56E+07	2.96E-11	2.44E-11	2.45E-11	2.47E-11	2.06E-10
Cm-248	3.48E+05	1.58E-10	1.25E-10	1.26E-10	1.27E-10	1.07E-09
Transuranic concentration (nCi/g) =		548	548	548	547	548
Lobe MWd =		28,894	27,967	27,978	28,017	For 8 blocks
Beryllium mass (g) =		81,420	81,420	81,420	81,420	651,360
Metal volume (m <sup>3</sup> ) =		0.0440	0.0440	0.0440	0.0440	0.3521
NE-L = northeast-left						
NE-R = northeast-right						
NW-L = northwest-left						
NW-R = northwest-right						
SE-L = southeast-left						
SE-R = southeast-right						
SW-L = southwest-left						
SW-R = southwest-right						

Table 7-9. Inventory calculated using Oak Ridge Isotope GENERation and Depletion Code Version 2 at the estimated disposal date of October 14 1982, for the Advanced Test Reactor beryllium blocks located in Core 2.

Isotope	Half-life (years)	Lobe NW	Lobe NE	Lobe SW	Lobe SE	Total for Six Blocks (NW blocks excluded) (Ci for six blocks)
		NW-L or NW-R (Ci per block)	NE-L or NE-R (Ci per block)	SW-L or SW-R (Ci per block)	SE-L or SE-R (Ci per block)	
H-3	1.23E+01	2.06+04	1.23E+04	2.04E+04	1.28E+04	9.09E+04
Be-10	1.60E+06	1.58E-01	1.02E-01	1.56E-01	1.05E-01	7.26E-01
C-14	5.73E+03	1.26E+00	8.18E-01	1.25E+00	8.44E-01	5.83E+00
Cl-36	3.01E+05	1.05E-02	6.93E-03	1.04E-02	7.13E-03	4.89E-02
Co-60	5.27E+00	1.05E+02	7.91E+01	1.04E+02	7.39E+01	5.00E+02
Ni-59	7.60E+04	2.40E-02	1.84E-02	2.39E-02	1.88E-02	1.22E-01
Ni-63	1.00E+02	4.54E+00	3.11E+00	4.51E+00	3.19E+00	2.16E+01
Sr-90	2.91E+01	3.93E-01	2.58E-01	3.90E-01	2.66E-01	1.83E+00
Nb-94	2.00E+04	2.78E-03	1.87E-03	2.76E-03	1.93E-03	1.31E-02
Tc-99	2.13E+05	1.61E-04	1.06E-04	1.60E-04	1.10E-04	7.51E-04
I-129	1.57E+07	1.19E-06	7.79E-07	1.18E-06	8.03E-07	5.53E-06
Cs-137	3.02E+01	1.30E+00	8.19E-01	1.29E+00	8.47E-01	5.91E+00
Eu-152	1.35E+01	9.18E-03	5.98E-02	9.56E-03	5.37E-02	2.46E-01
Eu-154	8.59E+00	1.53E+00	1.80E+00	1.54E+00	1.80E+00	1.03E+01
Pb-210	2.23E+01	3.93E-12	1.36E-12	3.86E-12	1.47E-12	1.34E-11
Ra-226	1.60E+03	1.00E-12	7.42E-13	9.98E-13	7.58E-13	5.00E-12
Ra-228	5.76E+00	2.19E-09	2.28E-09	2.19E-09	2.28E-09	1.35E-08
Ac-227	2.18E+01	6.56E-09	5.71E-09	6.55E-09	5.78E-09	3.61E-08
Th-228	1.91E+00	1.21E-05	6.76E-06	1.19E-05	7.07E-06	5.15E-05
Th-229	7.30E+03	5.79E-09	5.68E-09	5.79E-09	5.70E-09	3.43E-08
Th-230	7.54E+04	3.70E-10	2.77E-10	3.68E-10	2.83E-10	1.86E-09
Th-232	1.40E+10	3.44E-09	3.60E-09	3.44E-09	3.59E-09	2.13E-08
Pa-231	3.28E+04	3.18E-08	2.73E-08	3.17E-08	2.76E-08	1.73E-07
U-232	7.00E+01	1.30E-05	7.26E-06	1.28E-05	7.59E-06	5.54E-05
U-233	1.59E+05	7.81E-06	7.71E-06	7.81E-06	7.73E-06	4.65E-05
U-234	2.46E+05	2.01E-06	1.57E-06	2.00E-06	1.60E-06	1.04E-05
U-235	7.04E+08	2.31E-10	8.42E-10	2.35E-10	7.60E-10	3.67E-09
U-236	2.34E+07	1.39E-07	1.50E-07	1.39E-07	1.50E-07	8.78E-07
U-238	4.47E+09	6.48E-07	7.03E-07	6.49E-07	7.00E-07	4.10E-06
Np-237	2.14E+06	2.15E-07	1.83E-07	2.15E-07	1.86E-07	1.17E-06
Pu-238	8.77E+01	9.96E-03	8.94E-03	9.97E-03	9.11E-03	5.60E-02
Pu-239	2.41E+04	2.40E-03	2.58E-03	2.40E-03	2.57E-03	1.51E-02
Pu-240	6.56E+03	4.09E-03	4.20E-03	4.09E-03	4.19E-03	2.50E-02

Table 7-9. (continued).

Isotope	Half-life (years)	Lobe NW	Lobe NE	Lobe SW	Lobe SE	Total for Six Blocks (NW blocks excluded) (Ci for six blocks)
		NW-L or NW-R (Ci per block)	NE-L or NE-R (Ci per block)	SW-L or SW-R (Ci per block)	SE-L or SE-R (Ci per block)	
Pu-241	1.44E+01	8.20E-01	8.52E-01	8.21E-01	8.53E-01	5.05E+00
Pu-242	3.75E+05	7.91E-05	4.99E-05	7.86E-05	5.20E-05	3.61E-04
Pu-244	8.00E+07	1.04E-10	2.31E-11	1.01E-10	2.59E-11	3.00E-10
Am-241	4.33E+02	9.20E-03	9.96E-03	9.22E-03	9.94E-03	5.82E-02
Am-243	7.37E+03	9.10E-04	4.13E-04	8.99E-04	4.41E-04	3.51E-03
Cm-243	2.91E+01	2.67E-04	2.01E-04	2.66E-04	2.07E-04	1.35E-03
Cm-244	1.81E+01	3.06E-01	7.77E-02	3.00E-01	8.64E-02	9.27E-01
Cm-245	8.50E+03	1.83E-05	4.13E-06	1.79E-05	4.63E-06	5.33E-05
Cm-246	4.76E+03	2.48E-05	3.09E-06	2.40E-05	3.61E-06	6.13E-05
Cm-247	1.56E+07	1.10E-10	8.84E-12	1.06E-10	1.07E-11	2.50E-10
Cm-248	3.48E+05	7.90E-10	3.68E-11	7.50E-10	4.61E-11	1.67E-09
Transuranic concentration (nCi/g) =		3.31E+02	3.24E+02	3.31E+02	3.26E+02	3.27E+02
Lobe MWd =		36,569	23,625	36,285	24,357	For 6 blocks
Beryllium mass (g) =		81,420	81,420	81,420	81,420	488,520
Metal volume (m <sup>3</sup> ) =		0.0440	0.0440	0.0440	0.0440	0.2641

NE-L = northeast-left  
NE-R = northeast-right  
NW-L = northwest-left  
NW-R = northwest-right  
SE-L = southeast-left  
SE-R = southeast-right  
SW-L = southwest-left  
SW-R = southwest-right

Table 7-10. Inventory calculated using Oak Ridge Isotope Generation and Depletion Code Version 2 at the decay time of September 15, 2001, for the Advanced Test Reactor beryllium blocks located in Core 2.

Isotope	Half-life (years)	Lobe NW	Lobe NE	Lobe SW	Lobe SE	Total for Six Blocks (NW blocks excluded) (Ci for six blocks)
		NW-L or NW-R (Ci per block)	NE-L or NE-R (Ci per block)	SW-L or SW-R (Ci per block)	SE-L or SE-R (Ci per block)	
H-3	1.23E+01	7.12E+03	4.25E+03	7.06E+03	4.41E+03	3.14E+04
Be-10	1.60E+06	1.58E-01	1.02E-01	1.56E-01	1.05E-01	7.26E-01
C-14	5.73E+03	1.26E+00	8.17E-01	1.25E+00	8.42E-01	5.82E+00
Cl-36	3.01E+05	1.05E-02	6.93E-03	1.04E-02	7.13E-03	4.89E-02
Co-60	5.27E+00	8.71E+00	5.97E+00	8.65E+00	6.13E+00	4.15E+01
Ni-59	7.60E+04	2.40E-02	1.84E-02	2.39E-02	1.88E-02	1.22E-01
Ni-63	1.00E+02	3.94E+00	2.70E+00	3.91E+00	2.77E+00	1.88E+01
Sr-90	2.91E+01	2.51E-01	1.64E-01	2.49E-01	1.69E-01	1.16E+00
Nb-94	2.00E+04	2.78E-03	1.87E-03	2.76E-03	1.93E-03	1.31E-02
Tc-99	2.13E+05	1.61E-04	1.06E-04	1.60E-04	1.10E-04	7.52E-04

Table 7-10. (continued).

Isotope	Half-life (years)	Lobe NW	Lobe NE	Lobe SW	Lobe SE	Total for Six Blocks (NW blocks excluded)
		NW-L or NW-R (Ci per block)	NE-L or NE-R (Ci per block)	SW-L or SW-R (Ci per block)	SE-L or SE-R (Ci per block)	(Ci for six blocks)
I-129	1.57E+07	1.19E-06	7.79E-07	1.19E-06	8.03E-07	5.54E-06
Cs-137	3.02E+01	8.39E-01	5.29E-01	8.32E-01	5.47E-01	3.82E+00
Eu-152	1.35E+01	3.45E-03	2.25E-02	3.59E-03	2.02E-02	9.26E-02
Eu-154	8.59E+00	3.32E-01	3.90E-01	3.34E-01	3.89E-01	2.23E+00
Pb-210	2.23E+01	3.62E-12	1.84E-12	3.57E-12	1.92E-12	1.47E-11
Ra-226	1.60E+03	5.53E-12	4.20E-12	5.51E-12	4.28E-12	2.80E-11
Ra-228	5.76E+00	3.26E-09	3.41E-09	3.26E-09	3.40E-09	2.01E-08
Ac-227	2.18E+01	1.80E-08	1.55E-08	1.80E-08	1.57E-08	9.84E-08
Th-228	1.91E+00	1.11E-05	6.22E-06	1.10E-05	6.50E-06	4.74E-05
Th-229	7.30E+03	1.97E-08	1.94E-08	1.97E-08	1.96E-08	1.17E-07
Th-230	7.54E+04	7.55E-10	5.83E-10	7.52E-10	5.95E-10	3.86E-09
Th-232	1.40E+10	3.44E-09	3.60E-09	3.44E-09	3.59E-09	2.13E-08
Pa-231	3.28E+04	3.18E-08	2.72E-08	3.17E-08	2.76E-08	1.73E-07
U-232	7.00E+01	1.08E-05	6.06E-06	1.07E-05	6.33E-06	4.62E-05
U-233	1.59E+05	7.81E-06	7.71E-06	7.81E-06	7.73E-06	4.65E-05
U-234	2.46E+05	2.50E-06	2.02E-06	2.50E-06	2.06E-06	1.32E-05
U-235	7.04E+08	2.76E-10	8.90E-10	2.80E-10	8.08E-10	3.96E-09
U-236	2.34E+07	1.41E-07	1.53E-07	1.42E-07	1.52E-07	8.94E-07
U-238	4.47E+09	6.48E-07	7.03E-07	6.49E-07	7.00E-07	4.10E-06
Np-237	2.14E+06	3.28E-07	3.03E-07	3.28E-07	3.06E-07	1.87E-06
Pu-238	8.77E+01	8.58E-03	7.70E-03	8.59E-03	7.85E-03	4.83E-02
Pu-239	2.41E+04	2.40E-03	2.58E-03	2.40E-03	2.57E-03	1.51E-02
Pu-240	6.56E+03	4.52E-03	4.30E-03	4.51E-03	4.31E-03	2.62E-02
Pu-241	1.44E+01	3.30E-01	3.43E-01	3.30E-01	3.43E-01	2.03E+00
Pu-242	3.75E+05	7.91E-05	4.99E-05	7.86E-05	5.20E-05	3.61E-04
Pu-244	8.00E+07	1.04E-10	2.31E-11	1.01E-10	2.59E-11	3.00E-10
Am-241	4.33E+02	2.50E-02	2.63E-02	2.50E-02	2.63E-02	1.55E-01
Am-243	7.37E+03	9.08E-04	4.12E-04	8.98E-04	4.40E-04	3.50E-03
Cm-243	2.91E+01	1.68E-04	1.27E-04	1.68E-04	1.31E-04	8.52E-04
Cm-244	1.81E+01	1.48E-01	3.76E-02	1.45E-01	4.19E-02	4.49E-01
Cm-245	8.50E+03	1.83E-05	4.12E-06	1.79E-05	4.63E-06	5.33E-05
Cm-246	4.76E+03	2.47E-05	3.08E-06	2.39E-05	3.60E-06	6.12E-05
Cm-247	1.56E+07	1.10E-10	8.84E-12	1.06E-10	1.07E-11	2.51E-10

Table 7-10. (continued).

Isotope	Half-life (years)	Lobe NW	Lobe NE	Lobe SW	Lobe SE	Total for Six Blocks (NW blocks excluded)
		NW-L or NW-R (Ci per block)	NE-L or NE-R (Ci per block)	SW-L or SW-R (Ci per block)	SE-L or SE-R (Ci per block)	(Ci for six blocks)
Cm-248	3.48E+05	7.91E-10	3.69E-11	7.51E-10	4.62E-11	1.67E-09
Transuranic concentration (nCi/g) =		512	509	512	512	511
Lobe MWd =		36,569	23,625	36,285	24,357	For 6 blocks
Beryllium mass (g) =		81,420	81,420	81,420	81,420	488,520
Metal volume (m <sup>3</sup> ) =		0.0440	0.0440	0.0440	0.0440	0.2641
NE-L = northeast-left						
NE-R = northeast-right						
NW-L = northwest-left						
NW-R = northwest-right						
SE-L = southeast-left						
SE-R = southeast-right						
SW-L = southwest-left						
SW-R = southwest-right						

Table 7-11. Inventory calculated using Oak Ridge Isotope Generation and Depletion Code Version 2 at the estimated disposal date of July 1, 1993, for the Advanced Test Reactor beryllium blocks located in Core 3.

Isotope	Half-life (years)	NW-L or NW-R 018L and 013R (Ci per block)	NE-L or NE-R 015L (Ci per block)	SW-L or SW-R 019L and 014R (Ci per block)	SE-L or SE-R 011R (Ci per block)	Total for Six Blocks (Ci for six blocks)
H-3	1.23E+01	2.80E+04	2.42E+04	3.16E+04	3.89E+04	1.82E+05
Be-10	1.60E+06	2.32E-01	2.04E-01	2.60E-01	3.15E-01	1.50E+00
C-14	5.73E+03	1.85E+00	1.63E+00	2.07E+00	2.50E+00	1.20E+01
Cl-36	3.01E+05	1.50E-02	1.33E-02	1.65E-02	1.96E-02	9.59E-02
Co-60	5.27E+00	8.58E+01	7.76E+01	9.30E+01	1.06E+02	5.41E+02
Ni-59	7.60E+04	2.86E-02	2.71E-02	2.96E-02	3.12E-02	1.75E-01
Ni-63	1.00E+02	6.02E+00	5.43E+00	6.54E+00	7.49E+00	3.80E+01
Sr-90	2.91E+01	5.08E-01	4.52E-01	5.59E-01	6.56E-01	3.24E+00
Nb-94	2.00E+04	3.88E-03	3.48E-03	4.25E-03	4.95E-03	2.47E-02
Tc-99	2.13E+05	2.17E-04	1.97E-04	2.34E-04	2.63E-04	1.36E-03
I-129	1.57E+07	1.70E-06	1.51E-06	1.87E-06	2.20E-06	1.09E-05
Cs-137	3.02E+01	1.73E+00	1.53E+00	1.91E+00	2.27E+00	1.11E+01
Eu-152	1.35E+01	7.28E-04	1.61E-03	3.97E-04	1.91E-04	4.05E-03
Eu-154	8.59E+00	8.31E-01	9.60E-01	7.29E-01	5.76E-01	4.66E+00
Pb-210	2.23E+01	8.75E-12	6.61E-12	1.10E-11	1.61E-11	6.22E-11
Ra-226	1.60E+03	2.42E-12	2.26E-12	2.55E-12	2.77E-12	1.50E-11
Ra-228	5.76E+00	2.63E-09	2.69E-09	2.57E-09	2.46E-09	1.56E-08
Ac-227	2.18E+01	9.58E-09	9.60E-09	9.48E-09	9.13E-09	5.69E-08
Th-228	1.91E+00	1.87E-05	1.65E-05	2.05E-05	2.34E-05	1.18E-04
Th-229	7.30E+03	8.47E-09	8.54E-09	8.41E-09	8.31E-09	5.06E-08



Table 7-11. (continued).

Isotope	Half-life (years)	NW-L or NW-R 018L and 013R (Ci per block)	NE-L or NE-R 015L (Ci per block)	SW-L or SW-R 019L and 014R (Ci per block)	SE-L or SE-R 011R (Ci per block)	Total for Six Blocks (Ci for six blocks)
Th-230	7.54E+04	5.91E-10	5.56E-10	6.19E-10	6.64E-10	3.64E-09
Th-232	1.40E+10	3.23E-09	3.31E-09	3.16E-09	3.02E-09	1.91E-08
Pa-231	3.28E+04	3.35E-08	3.33E-08	3.35E-08	3.30E-08	2.00E-07
U-232	7.00E+01	1.89E-05	1.67E-05	2.07E-05	2.37E-05	1.20E-04
U-233	1.59E+05	7.18E-06	7.28E-06	7.08E-06	6.88E-06	4.27E-05
U-234	2.46E+05	2.23E-06	2.18E-06	2.27E-06	2.30E-06	1.35E-05
U-235	7.04E+08	1.70E-10	1.72E-10	1.72E-10	1.77E-10	1.03E-09
U-236	2.34E+07	1.23E-07	1.29E-07	1.18E-07	1.07E-07	7.18E-07
U-238	4.47E+09	5.81E-07	6.05E-07	5.58E-07	5.15E-07	3.40E-06
Np-237	2.14E+06	2.25E-07	2.29E-07	2.19E-07	2.05E-07	1.32E-06
Pu-238	8.77E+01	1.25E-02	1.36E-02	1.15E-02	9.73E-03	7.13E-02
Pu-239	2.41E+04	2.18E-03	2.24E-03	2.07E-03	1.91E-03	1.27E-02
Pu-240	6.56E+03	4.18E-03	4.16E-03	4.21E-03	4.28E-03	2.52E-02
Pu-241	1.44E+01	6.77E-01	7.02E-01	6.54E-01	6.09E-01	3.97E+00
Pu-242	3.75E+05	9.95E-05	9.35E-05	1.03E-04	1.07E-04	6.06E-04
Pu-244	8.00E+07	1.84E-10	1.28E-10	2.46E-10	3.98E-10	1.39E-09
Am-241	4.33E+02	1.08E-02	1.14E-02	1.03E-02	9.44E-03	6.30E-02
Am-243	7.37E+03	1.40E-03	1.24E-03	1.51E-03	1.65E-03	8.71E-03
Cm-243	2.91E+01	2.62E-04	2.70E-04	2.54E-04	2.35E-04	1.54E-03
Cm-244	1.81E+01	7.04E-01	5.26E-01	8.77E-01	1.22E+00	4.91E+00
Cm-245	8.50E+03	4.84E-05	3.55E-05	6.11E-05	8.69E-05	3.41E-04
Cm-246	4.76E+03	1.14E-04	6.95E-05	1.69E-04	3.18E-04	9.54E-04
Cm-247	1.56E+07	7.21E-10	3.92E-10	1.16E-09	2.52E-09	6.67E-09
Cm-248	3.48E+05	8.56E-09	3.92E-09	1.60E-08	4.48E-08	9.78E-08
Transuranic concentration (nCi/g) =		388	407	371	341	377
Lobe MWd =		53,924	47,259	60,205	72,984	For 6 blocks
Beryllium mass (g) =		81,420	81,420	81,420	81,420	488,520
Metal volume (m <sup>3</sup> ) =		0.0440	0.0440	0.0440	0.0440	0.2641
NE-L = northeast-left NE-R = northeast-right NW-L = northwest-left NW-R = northwest-right SE-L = southeast-left SE-R = southeast-right SW-L = southwest-left SW-R = southwest-right						

Table 7-12. Inventory calculated using Oak Ridge Isotope Generation and Depletion Code Version 2 at the decay time of September 15, 2001, for the Advanced Test Reactor beryllium blocks located in Core 3.

Isotope	Half-life (years)	NW-L or NW-R 018L and 013R (Ci per block)	NE-L or NE-R 015L (Ci per block)	SW-L or SW-R 019L and 014R (Ci per block)	SE-L or SE-R 011R (Ci per block)	Total for Six Blocks (Ci for six blocks)
Be-10	1.60E+06	2.32E-01	2.04E-01	2.60E-01	3.15E-01	1.50E+00
C-14	5.73E+03	1.85E+00	1.63E+00	2.06E+00	2.49E+00	1.19E+01
Cl-36	3.01E+05	1.50E-02	1.33E-02	1.65E-02	1.96E-02	9.59E-02
Co-60	5.27E+00	2.91E+01	2.64E+01	3.16E+01	3.61E+01	1.84E+02
Ni-59	7.60E+04	2.86E-02	2.71E-02	2.96E-02	3.12E-02	1.75E-01
Ni-63	1.00E+02	5.66E+00	5.11E+00	6.14E+00	7.04E+00	3.58E+01
Sr-90	2.91E+01	4.18E-01	3.72E-01	4.60E-01	5.40E-01	2.67E+00
Nb-94	2.00E+04	3.88E-03	3.48E-03	4.25E-03	4.95E-03	2.47E-02
Tc-99	2.13E+05	2.17E-04	1.97E-04	2.34E-04	2.63E-04	1.36E-03
I-129	1.57E+07	1.70E-06	1.51E-06	1.87E-06	2.20E-06	1.09E-05
Cs-137	3.02E+01	1.43E+00	1.26E+00	1.58E+00	1.88E+00	9.16E+00
Eu-152	1.35E+01	4.79E-04	1.06E-03	2.61E-04	1.23E-04	2.66E-03
Eu-154	8.59E+00	4.29E-01	4.95E-01	3.76E-01	2.97E-01	2.40E+00
Pb-210	2.23E+01	7.59E-12	5.88E-12	9.37E-12	1.34E-11	5.32E-11
Ra-226	1.60E+03	4.81E-12	4.53E-12	5.05E-12	5.43E-12	2.97E-11
Ra-228	5.76E+00	2.97E-09	3.04E-09	2.91E-09	2.78E-09	1.76E-08
Ac-227	2.18E+01	1.51E-08	1.50E-08	1.50E-08	1.46E-08	8.98E-08
Th-228	1.91E+00	1.78E-05	1.58E-05	1.96E-05	2.24E-05	1.13E-04
Th-229	7.30E+03	1.40E-08	1.42E-08	1.39E-08	1.36E-08	8.36E-08
Th-230	7.54E+04	7.66E-10	7.28E-10	7.95E-10	8.42E-10	4.69E-09
Th-232	1.40E+10	3.23E-09	3.31E-09	3.16E-09	3.02E-09	1.91E-08
Pa-231	3.28E+04	3.35E-08	3.33E-08	3.35E-08	3.30E-08	2.00E-07
U-232	7.00E+01	1.74E-05	1.54E-05	1.91E-05	2.19E-05	1.10E-04
U-233	1.59E+05	7.18E-06	7.28E-06	7.08E-06	6.88E-06	4.27E-05
U-234	2.46E+05	2.51E-06	2.48E-06	2.52E-06	2.51E-06	1.51E-05
U-235	7.04E+08	1.87E-10	1.91E-10	1.89E-10	1.92E-10	1.14E-09
U-236	2.34E+07	1.24E-07	1.30E-07	1.19E-07	1.09E-07	7.25E-07
U-238	4.47E+09	5.81E-07	6.05E-07	5.58E-07	5.15E-07	3.40E-06
Np-237	2.14E+06	2.64E-07	2.70E-07	2.57E-07	2.39E-07	1.55E-06
Pu-238	8.77E+01	1.17E-02	1.28E-02	1.07E-02	9.12E-03	6.67E-02
Pu-239	2.41E+04	2.15E-03	2.24E-03	2.07E-03	1.91E-03	1.26E-02
Pu-240	6.56E+03	4.71E-03	4.55E-03	4.86E-03	5.19E-03	2.89E-02
Pu-241	1.44E+01	4.56E-01	4.73E-01	4.41E-01	4.10E-01	2.68E+00
Pu-242	3.75E+05	9.95E-05	9.35E-05	1.03E-04	1.07E-04	6.06E-04
Pu-244	8.00E+07	1.84E-10	1.28E-10	2.46E-10	3.98E-10	1.39E-09
Am-241	4.33E+02	1.80E-02	1.88E-02	1.73E-02	1.59E-02	1.05E-01
Am-243	7.37E+03	1.40E-03	1.24E-03	1.51E-03	1.65E-03	8.71E-03

Table 7-12. (continued).

Isotope	Half-life (years)	NW-L or NW-R 018L and 013R (Ci per block)	NE-L or NE-R 015L (Ci per block)	SW-L or SW-R 019L and 014R (Ci per block)	SE-L or SE-R 011R (Ci per block)	Total for Six Blocks (Ci for six blocks)
Cm-243	2.91E+01	2.15E-04	2.21E-04	2.08E-04	1.93E-04	1.26E-03
Cm-244	1.81E+01	5.14E-01	3.84E-01	6.40E-01	8.94E-01	3.59E+00
Cm-245	8.50E+03	4.84E-05	3.55E-05	6.11E-05	8.68E-05	3.41E-04
Cm-246	4.76E+03	1.14E-04	6.94E-05	1.69E-04	3.18E-04	9.53E-04
Cm-247	1.56E+07	7.21E-10	3.92E-10	1.16E-09	2.52E-09	6.67E-09
Cm-248	3.48E+05	8.57E-09	3.92E-09	1.60E-08	4.49E-08	9.80E-08
Transuranic concentration (nCi/g) =		473	493	455	424	462
Lobe MWd =		53,924	47,259	60,205	72,984	For 6 blocks
Beryllium mass (g) =		81,420	81,420	81,420	81,420	488,520
Metal volume (m <sup>3</sup> ) =		0.0440	0.0440	0.0440	0.0440	0.2641

NE-L = northeast-left  
NE-R = northeast-right  
NW-L = northwest-left  
NW-R = northwest-right  
SE-L = southeast-left  
SE-R = southeast-right  
SW-L = southwest-left  
SW-R = southwest-right

Table 7-13. Inventory calculated using Oak Ridge Isotope Generation and Depletion Code Version 2 at the estimated disposal date of September 1, 1987, for the outer shim control cylinders located in Cores 1 and 2.

Isotope	Half-life (years)	Total Inventory for 16 OSCCs (Ci per 16 OSCCs)	Inventory for Nine of the 16 OSCCs (Ci per nine OSCCs)
H-3	1.23E+01	1.53E+05	8.61E+04
Be-10	1.60E+06	3.57E+00	2.01E+00
C-14	5.73E+03	2.83E+01	1.59E+01
Cl-36	3.01E+05	1.72E-01	9.68E-02
Co-60	5.27E+00	7.38E+02	4.15E+02
Ni-59	7.60E+04	3.45E-01	1.94E-01
Ni-63	1.00E+02	8.13E+01	4.57E+01
Sr-90	2.91E+01	5.33E+00	3.00E+00
Nb-94	2.00E+04	4.98E-02	2.80E-02
Tc-99	2.13E+05	2.40E-03	1.35E-03
I-129	1.57E+07	1.94E-05	1.09E-05
Cs-137	3.02E+01	1.83E+01	1.03E+01
Eu-152	1.35E+01	5.29E-03	2.98E-03
Eu-154	8.59E+00	6.39E+00	3.59E+00
Pb-210	2.23E+01	6.20E-11	3.49E-11
Ra-226	1.60E+03	2.72E-11	1.53E-11
Ra-228	5.76E+00	2.90E-08	1.63E-08
Ac-227	2.18E+01	7.23E-08	4.07E-08

Table 7-13. (continued).

Isotope	Half-life (years)	Total Inventory for 16 OSCCs (Ci per 16 OSCCs)	Inventory for Nine of the 16 OSCCs (Ci per nine OSCCs)
Th-228	1.91E+00	1.23E-04	6.92E-05
Th-229	7.30E+03	9.48E-08	5.33E-08
Th-230	7.54E+04	5.66E-09	3.18E-09
Th-232	1.40E+10	3.32E-08	1.87E-08
Pa-231	3.28E+04	2.06E-07	1.16E-07
U-232	7.00E+01	1.21E-04	6.81E-05
U-233	1.59E+05	6.63E-05	3.73E-05
U-234	2.46E+05	2.23E-05	1.25E-05
U-235	7.04E+08	1.58E-09	8.89E-10
U-236	2.34E+07	1.26E-06	7.09E-07
U-238	4.47E+09	6.12E-06	3.44E-06
Np-237	2.14E+06	1.87E-06	1.05E-06
Pu-238	8.77E+01	7.61E-02	4.28E-02
Pu-239	2.41E+04	1.72E-02	9.68E-03
Pu-240	6.56E+03	4.39E-02	2.47E-02
Pu-241	1.44E+01	4.45E+00	2.50E+00
Pu-242	3.75E+05	1.06E-03	5.96E-04
Pu-244	8.00E+07	3.09E-09	1.74E-09
Am-241	4.33E+02	1.02E-01	5.74E-02
Am-243	7.37E+03	1.46E-02	8.21E-03
Cm-243	2.91E+01	1.60E-03	9.00E-04
Cm-244	1.81E+01	7.84E+00	4.41E+00
Cm-245	8.50E+03	4.60E-04	2.59E-04
Cm-246	4.76E+03	1.77E-03	9.96E-04
Cm-247	1.56E+07	1.10E-08	6.19E-09
Cm-248	3.48E+05	2.00E-07	1.13E-07
Transuranic concentration (nCi/g) =		297	297
		Total for 16 OSCCs	Total for Nine OSCCs
Beryllium mass (g) =		870,900	489,880
Metal volume (m <sup>3</sup> ) =		0.4708	0.2648

OSCC = outer shim control cylinder

Table 7-14. Inventory calculated using Oak Ridge Isotope Generation and Depletion Code Version 2 at the decay time of September 15, 2001, for the outer shim control cylinders located in Cores 1 and 2.

Isotope	Half-life (years)	Total Inventory for 16 OSCCs (Ci per 16 OSCCs)	Inventory for Nine of the 16 OSCCs (Ci per nine OSCCs)
H-3	1.23E+01	6.96E+04	3.92E+04
Be-10	1.60E+06	3.57E+00	2.01E+00
C-14	5.73E+03	2.83E+01	1.59E+01
Cl-36	3.01E+05	1.72E-01	9.68E-02
Co-60	5.27E+00	1.16E+02	6.53E+01

Table 7-14. (continued).

Isotope	Half-life (years)	Total Inventory for 16 OSCCs (Ci per 16 OSCCs)	Inventory for Nine of the 16 OSCCs (Ci per nine OSCCs)
Ni-59	7.60E+04	3.45E-01	1.94E-01
Ni-63	1.00E+02	7.32E+01	4.12E+01
Sr-90	2.91E+01	3.82E+00	2.15E+00
Nb-94	2.00E+04	4.98E-02	2.80E-02
Tc-99	2.13E+05	2.40E-03	1.35E-03
I-129	1.57E+07	1.94E-05	1.09E-05
Cs-137	3.02E+01	1.32E+01	7.43E+00
Eu-152	1.35E+01	2.59E-03	1.46E-03
Eu-154	8.59E+00	2.06E+00	1.16E+00
Pb-210	2.23E+01	5.73E-11	3.22E-11
Ra-226	1.60E+03	7.03E-11	3.95E-11
Ra-228	5.76E+00	3.22E-08	1.81E-08
Ac-227	2.18E+01	1.21E-07	6.81E-08
Th-228	1.91E+00	1.09E-04	6.13E-05
Th-229	7.30E+03	1.83E-07	1.03E-07
Th-230	7.54E+04	8.66E-09	4.87E-09
Th-232	1.40E+10	3.32E-08	1.87E-08
Pa-231	3.28E+04	2.06E-07	1.16E-07
U-232	7.00E+01	1.06E-04	5.99E-05
U-233	1.59E+05	6.63E-05	3.73E-05
U-234	2.46E+05	2.52E-05	1.42E-05
U-235	7.04E+08	1.82E-09	1.02E-09
U-236	2.34E+07	1.28E-06	7.20E-07
U-238	4.47E+09	6.12E-06	3.44E-06
Np-237	2.14E+06	2.51E-06	1.41E-06
Pu-238	8.77E+01	6.81E-02	3.83E-02
Pu-239	2.41E+04	1.72E-02	9.68E-03
Pu-240	6.56E+03	5.28E-02	2.97E-02
Pu-241	1.44E+01	2.26E+00	1.27E+00
Pu-242	3.75E+05	1.06E-03	5.96E-04
Pu-244	8.00E+07	3.09E-09	1.74E-09
Am-241	4.33E+02	1.72E-01	9.68E-02
Am-243	7.37E+03	1.45E-02	8.16E-03
Cm-243	2.91E+01	1.14E-03	6.41E-04
Cm-244	1.81E+01	4.58E+00	2.58E+00
Cm-245	8.50E+03	4.59E-04	2.58E-04

Table 7-14. (continued).

Isotope	Half-life (years)	Total Inventory for 16 OSCCs (Ci per 16 OSCCs)	Inventory for Nine of the 16 OSCCs (Ci per nine OSCCs)
Cm-246	4.76E+03	1.77E-03	9.96E-04
Cm-247	1.56E+07	1.10E-08	6.19E-09
Cm-248	3.48E+05	2.01E-07	1.13E-07
Transuranic concentration (nCi/g) =		378	378
		Total for 16 OSCCs	Total for Nine OSCCs
Beryllium mass (g) =		870,900	489,880
Metal volume (m <sup>3</sup> ) =		0.4708	0.2648

OSCC = outer shim control cylinder

Table 7-15. Data computed using Oak Ridge Isotope Generation and Depletion Code Version 2 at the time of disposal for beryllium from the Advanced Test Reactor.

Isotope	Half-life (years)	12/01/76	10/14/82	07/01/93	09/01/87	Total Inventory for 20 Blocks and Nine OSCCs (Ci total)
		Eight Buried Blocks from Core 1 (Ci for eight blocks)	Six Buried Blocks from Core 2 (Ci for six blocks)	Six Buried Blocks from Core 3 (Ci for six blocks)	Nine of the 16 OSCCs from Cores 1 and 2 (Ci per nine OSCCs)	
H-3	1.23E+01	1.31E+05	9.09E+04	1.82E+05	8.61E+04	4.90E+05
Be-10	1.60E+06	9.76E-01	7.26E-01	1.50E+00	2.01E+00	5.21E+00
C-14	5.73E+03	7.81E+00	5.83E+00	1.20E+01	1.59E+01	4.15E+01
Cl-36	3.01E+05	6.56E-02	4.89E-02	9.59E-02	9.68E-02	3.07E-01
Co-60	5.27E+00	7.75E+02	5.00E+02	5.41E+02	4.15E+02	2.23E+03
Ni-59	7.60E+04	1.65E-01	1.22E-01	1.75E-01	1.94E-01	6.56E-01
Ni-63	1.00E+02	2.93E+01	2.16E+01	3.80E+01	4.57E+01	1.35E+02
Sr-90	2.91E+01	2.52E+00	1.83E+00	3.24E+00	3.00E+00	1.06E+01
Nb-94	2.00E+04	1.76E-02	1.31E-02	2.47E-02	2.80E-02	8.34E-02
Tc-99	2.13E+05	1.02E-03	7.51E-04	1.36E-03	1.35E-03	4.48E-03
I-129	1.57E+07	7.44E-06	5.53E-06	1.09E-05	1.09E-05	3.48E-05
Cs-137	3.02E+01	8.12E+00	5.91E+00	1.11E+01	1.03E+01	3.54E+01
Eu-152	1.35E+01	2.54E-01	2.46E-01	4.05E-03	2.98E-03	5.07E-01
Eu-154	8.59E+00	1.52E+01	1.03E+01	4.66E+00	3.59E+00	3.38E+01
Pb-210	2.23E+01	1.74E-11	1.34E-11	6.22E-11	3.49E-11	1.28E-10
Ra-226	1.60E+03	5.71E-12	5.00E-12	1.50E-11	1.53E-11	4.10E-11
Ra-228	5.76E+00	1.70E-08	1.35E-08	1.56E-08	1.63E-08	6.24E-08
Ac-227	2.18E+01	4.24E-08	3.61E-08	5.69E-08	4.0E-08	1.75E-07
Th-228	1.91E+00	6.64E-05	5.15E-05	1.18E-04	6.92E-05	3.05E-04
Th-229	7.30E+03	3.98E-08	3.43E-08	5.06E-08	5.33E-08	1.78E-07
Th-230	7.54E+04	2.40E-09	1.86E-09	3.64E-09	3.18E-09	1.11E-08
Th-232	1.40E+10	2.83E-08	2.13E-08	1.91E-08	1.87E-08	8.74E-08
Pa-231	3.28E+04	2.35E-07	1.73E-07	2.00E-07	1.16E-07	7.24E-07

Table 7-15. (continued).

Isotope	Half-life (years)	12/01/76	10/14/82	07/01/93	09/01/87	Total Inventory for 20 Blocks and Nine OSCCs (Ci total)
		Eight Buried Blocks from Core 1 (Ci for eight blocks)	Six Buried Blocks from Core 2 (Ci for six blocks)	Six Buried Blocks from Core 3 (Ci for six blocks)	Nine of the 16 OSCCs from Cores 1 and 2 (Ci per nine OSCCs)	
U-232	7.00E+01	7.53E-05	5.54E-05	1.20E-04	6.81E-05	3.19E-04
U-233	1.59E+05	6.19E-05	4.65E-05	4.27E-05	3.73E-05	1.88E-04
U-234	2.46E+05	1.36E-05	1.04E-05	1.35E-05	1.25E-05	5.00E-05
U-235	7.04E+08	3.69E-09	3.67E-09	1.03E-09	8.89E-10	9.28E-09
U-236	2.34E+07	1.17E-06	8.78E-07	7.18E-07	7.09E-07	3.48E-06
U-238	4.47E+09	5.46E-06	4.10E-06	3.40E-06	3.44E-06	1.64E-05
Np-237	2.14E+06	1.57E-06	1.17E-06	1.32E-06	1.05E-06	5.11E-06
Pu-238	8.77E+01	8.42E-02	5.60E-02	7.13E-02	4.28E-02	2.54E-01
Pu-239	2.41E+04	2.01E-02	1.51E-02	1.27E-02	9.68E-03	5.76E-02
Pu-240	6.56E+03	3.32E-02	2.50E-02	2.52E-02	2.47E-02	1.08E-01
Pu-241	1.44E+01	7.21E+00	5.05E+00	3.97E+00	2.50E+00	1.87E+01
Pu-242	3.75E+05	4.94E-04	3.61E-04	6.06E-04	5.96E-04	2.06E-03
Pu-244	8.00E+07	3.23E-10	3.00E-10	1.39E-09	1.74E-09	3.75E-09
Am-241	4.33E+02	6.49E-02	5.82E-02	6.30E-02	5.74E-02	2.44E-01
Am-243	7.37E+03	4.74E-03	3.51E-03	8.71E-03	8.21E-03	2.52E-02
Cm-243	2.91E+01	2.00E-03	1.35E-03	1.54E-03	9.00E-04	5.79E-03
Cm-244	1.81E+01	1.18E+00	9.27E-01	4.91E+00	4.41E+00	1.14E+01
Cm-245	8.50E+03	6.31E-05	5.33E-05	3.41E-04	2.59E-04	7.16E-04
Cm-246	4.76E+03	6.00E-05	6.13E-05	9.54E-04	9.96E-04	2.07E-03
Cm-247	1.56E+07	2.06E-10	2.50E-10	6.67E-09	6.19E-09	1.33E-08
Cm-248	3.48E+05	1.07E-09	1.67E-09	9.78E-08	1.13E-07	2.14E-07
Average transuranic concentration (nCi/g) =		322	327	377	297	330
Beryllium mass (g) =		651,360	488,520	488,520	489,881	2,118,281
Metal volume (m <sup>3</sup> ) =		0.352	0.264	0.264	0.265	1.145

OSCC = outer shim control cylinder

Table 7-16. Data computed using Oak Ridge Isotope Generation and Depletion Code Version 2 at the decay time of September 15, 2001, for disposal of beryllium from the Advanced Test Reactor.

Isotope	Half-life (years)	09/15/01	09/15/01	09/15/01	09/15/01	Total Inventory for 20 Blocks and Nine OSCCs (Ci total)
		Eight Buried Blocks from Core 1 (Ci for eight blocks)	Six Buried Blocks from Core 2 (Ci for six blocks)	Six Buried Blocks from Core 3 (Ci for six blocks)	Nine of the 16 OSCCs from Cores 1 and 2 (Ci per nine OSCCs)	
H-3	1.23E+01	3.24E+04	3.14E+04	1.15E+05	3.92E+04	2.18E+05
Be-10	1.60E+06	9.76E-01	7.26E-01	1.50E+00	2.01E+00	5.21E+00
C-14	5.73E+03	7.79E+00	5.82E+00	1.19E+01	1.59E+01	4.14E+01

Table 7-16. (continued).

Isotope	Half-life (years)	09/15/01	09/15/01	09/15/01	09/15/01	Total Inventory for 20 Blocks and Nine OSCCs (Ci total)
		Eight Buried Blocks from Core 1 (Ci for eight blocks)	Six Buried Blocks from Core 2 (Ci for six blocks)	Six Buried Blocks from Core 3 (Ci for six blocks)	Nine of the 16 OSCCs from Cores 1 and 2 (Ci per nine OSCCs)	
Cl-36	3.01E+05	6.56E-02	4.89E-02	9.59E-02	9.68E-02	3.07E-01
Co-60	5.27E+00	2.98E+01	4.15E+01	1.84E+02	6.53E+01	3.21E+02
Ni-59	7.60E+04	1.65E-01	1.22E-01	1.75E-01	1.94E-01	6.56E-01
Ni-63	1.00E+02	2.43E+01	1.88E+01	3.58E+01	4.12E+01	1.20E+02
Sr-90	2.91E+01	1.40E+00	1.16E+00	2.67E+00	2.15E+00	7.38E+00
Nb-94	2.00E+04	1.76E-02	1.31E-02	2.47E-02	2.80E-02	8.34E-02
Tc-99	2.13E+05	1.02E-03	7.52E-04	1.36E-03	1.35E-03	4.48E-03
I-129	1.57E+07	7.44E-06	5.54E-06	1.09E-05	1.09E-05	3.48E-05
Cs-137	3.02E+01	4.59E+00	3.82E+00	9.16E+00	7.43E+00	2.50E+01
Eu-152	1.35E+01	7.17E-02	9.26E-02	2.66E-03	1.46E-03	1.68E-01
Eu-154	8.59E+00	2.07E+00	2.23E+00	2.40E+00	1.16E+00	7.86E+00
Pb-210	2.23E+01	2.27E-11	1.47E-11	5.32E-11	3.22E-11	1.23E-10
Ra-226	1.60E+03	4.96E-11	2.80E-11	2.97E-11	3.95E-11	1.47E-10
Ra-228	5.76E+00	2.75E-08	2.01E-08	1.76E-08	1.81E-08	8.33E-08
Ac-227	2.18E+01	1.48E-07	9.84E-08	8.98E-08	6.81E-08	4.04E-07
Th-228	1.91E+00	6.10E-05	4.74E-05	1.13E-04	6.13E-05	2.83E-04
Th-229	7.30E+03	1.84E-07	1.17E-07	8.36E-08	1.03E-07	4.88E-07
Th-230	7.54E+04	6.03E-09	3.86E-09	4.69E-09	4.87E-09	1.95E-08
Th-232	1.40E+10	2.83E-08	2.13E-08	1.91E-08	1.87E-08	8.74E-08
Pa-231	3.28E+04	2.35E-07	1.73E-07	2.00E-07	1.16E-07	7.24E-07
U-232	7.00E+01	5.94E-05	4.62E-05	1.10E-04	5.99E-05	2.76E-04
U-233	1.59E+05	6.19E-05	4.65E-05	4.27E-05	3.73E-05	1.88E-04
U-234	2.46E+05	1.89E-05	1.32E-05	1.51E-05	1.42E-05	6.14E-05
U-235	7.04E+08	4.18E-09	3.96E-09	1.14E-09	1.02E-09	1.03E-08
U-236	2.34E+07	1.20E-06	8.94E-07	7.25E-07	7.20E-07	3.54E-06
U-238	4.47E+09	5.46E-06	4.10E-06	3.40E-06	3.44E-06	1.64E-05
Np-237	2.14E+06	2.88E-06	1.87E-06	1.55E-06	1.41E-06	7.71E-06
Pu-238	8.77E+01	6.90E-02	4.83E-02	6.67E-02	3.83E-02	2.22E-01
Pu-239	2.41E+04	2.01E-02	1.51E-02	1.26E-02	9.68E-03	5.75E-02
Pu-240	6.56E+03	3.51E-02	2.62E-02	2.89E-02	2.97E-02	1.20E-01
Pu-241	1.44E+01	2.19E+00	2.03E+00	2.68E+00	1.277E+00	8.18E+00
Pu-242	3.75E+05	4.94E-04	3.61E-04	6.06E-04	5.96E-04	2.06E-03
Pu-244	8.00E+07	3.23E-10	3.00E-10	1.39E-09	1.74E-09	3.75E-09
Am-241	4.33E+02	2.26E-01	1.55E-01	1.05E-01	9.68E-02	5.83E-01
Am-243	7.37E+03	4.72E-03	3.50E-03	8.67E-03	8.16E-03	2.51E-02
Cm-243	2.91E+01	1.09E-03	8.52E-04	1.26E-03	6.41E-04	3.84E-03



Table 7-16. (continued).

Isotope	Half-life (years)	09/15/01	09/15/01	09/15/01	09/15/01	Total Inventory for 20 Blocks and Nine OSCCs (Ci total)
		Eight Buried Blocks from Core 1 (Ci for eight blocks)	Six Buried Blocks from Core 2 (Ci for six blocks)	Six Buried Blocks from Core 3 (Ci for six blocks)	Nine of the 16 OSCCs from Cores 1 and 2 (Ci per nine OSCCs)	
Cm-244	1.81E+01	4.57E-01	4.49E-01	3.59E+00	2.58E+00	7.08E+00
Cm-245	8.50E+03	6.30E-05	5.33E-05	3.41E-04	2.58E-04	7.15E-04
Cm-246	4.76E+03	5.98E-05	6.12E-05	9.53E-04	9.96E-04	2.07E-03
Cm-247	1.56E+07	2.06E-10	2.51E-10	6.67E-09	6.19E-09	1.33E-08
Cm-248	3.48E+05	1.07E-09	1.67E-09	9.80E-08	1.13E-07	2.14E-07
Average transuranic concentration (nCi/g) =		548	511	461	378	480
Beryllium mass (g) =		651,360	488,520	488,520	489,881	2,118,281
Metal volume (m <sup>3</sup> ) =		0.352	0.264	0.264	0.265	1.145

OSCC = outer shim control cylinder

## 7.9 Analysis of Beryllium Reflectors from the Materials Test Reactor and the Engineering Test Reactor

The ETR and MTR beryllium reflectors and the reflector in the ATR have a number of similarities:

- All cores are approximately the same size. The ATR core is a little taller than the other two, but about the same nominal lateral dimension as the ETR. The MTR core was smaller and more elongated. ATR fuel is in a serpentine pattern while ETR fuel is essentially a 10 × 10 element square grid with fuel in some locations replaced by test loops. MTR fuel was a 5 × 9 array of nominally 7.6-cm (3-in.) square fuel elements 40 × 73 cm (15.7 × 28.8 in.). Additional details of the MTR and ETR can be found in the *Directory of Nuclear Reactors* (IAEA 1959; IAEA 1964).
- All beryllium reflectors are nominally the same height as the fuel elements.
- The ATR and ETR reflectors are close to the fuel, though ETR configuration is nominally square while ATR configuration provides a transition between the serpentine core and the cylindrical housing. The outer part of the MTR reflector was more removed from the fuel, as shown in Figure 3-1.
- All reflectors (counting the OSCCs in ATR) have approximately the same effective thickness from the fuel to the surroundings, though ETR is slightly thinner than the other two.
- None of the three reactors uses a top or bottom reflector, other than water coolant.
- Both ATR and ETR reactors appear to have operated at about half the rated power. The MTR reactor operated at its rated power for most of its life. However, because of a relatively low operating time, average power was less than one-third of rated power over the last half of its life.

- All of the beryllium reflectors appear to be made of very similar material, which would imply similar impurities.
- Neutron energy spectra are probably quite similar for each of the reactors, though the spectrum is probably more thermalized in the MTR reflector than in the ATR and ETR reflectors.
- The overall vertical spatial distribution of flux in all three reactors is probably quite similar.

The MTR first went critical on March 31, 1952, and first reached its designed operating power of 30 MW<sub>th</sub> on May 22, 1952. It operated at nominally the 30-MW<sub>th</sub> power level for about 40 months, until September 1955. Then the reactor was found to operate satisfactorily at 40 MW<sub>th</sub> and operated at that level until being shut down on July 3, 1969. During the shutdown, the original beryllium reflector was replaced and the enriched uranium fuel was removed. In late 1969, a second beryllium reflector and a new plutonium fuel core were installed. This second beryllium reflector is still inside the shut down reactor. The MTR operated using the replacement reflector from December 1969 until April 1970 and for about 3 days in August 1970 using a plutonium fuel (Rolfe and Wills 1984, Chapter 2). The total amount of energy that was generated in the MTR from May 22, 1952, until July 3, 1969, (i.e., Cycle 1 through 295) was 177,887 MWd (Ford et al. 1969). A slightly larger value of 179,323 MWd is reported by Rolfe and Wills (1984); however, Rolfe and Wills report this value being generated through about Cycle 305 (until mid 1969). For the current analysis, a value of 177,887 MWd was assumed to be uniformly generated during the entire 6,303 days of MTR operation, a period of time that used the first beryllium reflector. That is, an average reactor power of 28.22 MW (= 177,887 MWd/6,303 days) is assumed for each of 6,303 days of operation of MTR. In addition to energy generation, total neutron flux (i.e., fast+thermal) per MW of reactor power and total beryllium mass were determined in order to use ORIGEN2 for calculations. A beryllium mass of about 2,608 kg (5,750 lb) is reported by Rolfe and Wills (1984); however, this value appears to be too high (e.g., the beryllium would have to occupy the entire MTR core and reflector volumes). A more reasonable mass number can be estimated based on the physical dimensions of the reflector as reported in Volume II of the *Directory of Nuclear Reactors* (IAEA 1959). Calculations of MTR reflector volume (taking into consideration void spaces for beam ports) indicate that reflector metal volume ranges from 934,000 to 1,174,000 cm<sup>3</sup>. The average metal volume is ~1,054,000 cm<sup>3</sup>. Using a nominal beryllium density of 1.85 g/cm<sup>3</sup>, an average beryllium mass of ~2,000,000 g can be determined to one significant decimal place. The estimated uncertainty associated with the calculated MTR beryllium mass number is ±14%.

The fast and thermal neutron fluxes for each major reflector component are reported in Volume II of the *Directory of Nuclear Reactors* (IAEA 1959) for the MTR at a nominal reactor power of 40 MW. An average value of the fast and thermal neutron fluxes can be determined by averaging the individual reflector components. The total flux is then the sum of the fast and thermal components. The best-estimate total neutron flux for the MTR reflector (at 40 MW), computed to one significant decimal place, is  $1 \times 10^{14}$  n/cm<sup>2</sup>/second. Since the average MTR power was previously determined to be 28.22 MW, the time-averaged (steady-state) neutron flux is  $7.056 \times 10^{13}$  n/cm<sup>2</sup>/second.

In addition to the neutron flux, beryllium mass, and average reactor power, the elemental composition of beryllium reflector material (both major and trace elements) was estimated based on chemical assay data. The results of this analysis—applicable to both the MTR and ETR reflectors—are shown in Table 7-17. These data assume that both beryllium reflectors were made from KBI beryllium; however, trace element information from Brush Wellman assay data was used whenever KBI data were not available. In general, it is not known which company actually supplied the beryllium for the initial MTR and ETR core loadings although the second reflector for ETR was made by Brush Wellman using S-200 E-grade material (see drawing number 400883).

Using the above (steady-state) neutron flux (i.e.,  $7.056 \times 10^{13}$  n/cm<sup>2</sup>/second) computed at the beryllium reflector, the total irradiation time (6,303 days from May 22, 1952, until July 3, 1969), and the estimated beryllium mass (2,000,000 g), an ORIGEN2 computer model was produced for the MTR reflector. Around April 1970, 616,000 g (30.8%) of the MTR beryllium was disposed of. The remainder—1,384,000 grams (69.2%)—was disposed of in July 1977. The results of the ORIGEN2 calculation for selected radionuclides are listed in Table 7-18. Note that the calculated C-14 inventory for the MTR beryllium reflector at the time of disposal of this material at the SDA is 29.2 Ci. The calculated C-14 inventory for MTR also is shown in Table 1-1.

ETR first went critical in October 1957 with full power being achieved in April 1958 (Kaiser et al. 1982, IAEA 1964). The reflector was replaced in March 1970 (Kaiser et al. 1982). In May 1973, ETR's mission changed from thermal-hydraulic testing to research of fast breeder reactor issues. During its lifetime, the first reflector in the ETR experienced the same kind of testing operations. The length of time that ETR was operated with the first beryllium reflector installed in the reactor (e.g., Core 1) was about 4,520 days (i.e., October 15, 1957, to March 1, 1970). The total energy generated during this time is estimated to be 380,000 MWd and is based on a value extrapolation of 374,498 MWd reported for January 11, 1970, by E. H. Smith et al. (1970). An axially averaged total neutron flux of  $4.93 \times 10^{14}$  n/cm<sup>2</sup>/second (at 175 MW or  $2.817 \times 10^{14}$  n/cm<sup>2</sup>/second per MW) computed at the ETR beryllium reflector, was estimated from neutron flux data reported in Volume V of the *Directory of Nuclear Reactors* (IAEA 1964). For example, the thermal flux was determined to be the average of two values mentioned for the 1.3-in. diameter beryllium access holes:  $2 \times 10^{14}$  and  $6 \times 10^{14}$  n/cm<sup>2</sup>/second. Hence,  $\phi_{th} = 4.0 \times 10^{14}$  n/cm<sup>2</sup>/second (at 175 MW). The fast neutron flux ( $\phi_{fast}$ ) was determined by estimating the ratio of the fast to thermal flux ( $\phi_{fast} / \phi_{th} = \sim 2/3$ ) and then multiplying the thermal flux by this ratio. Hence, the total peak flux within the ETR beryllium reflector at 175 MW is:  $\phi_{peak} = \phi_{th} + \phi_{fast} = 4 \times 10^{14} + 2.7 \times 10^{14} = 6.7 \times 10^{14}$  n/cm<sup>2</sup>/second. The axial peak power to average core power ratio for ETR is  $\sim 1.36$ . Therefore, the average axial total neutron flux at the ETR beryllium reflector is computed as:  $\phi_{total} = \phi_{peak} / 1.36 = 6.7 \times 10^{14} / 1.36 = 4.93 \times 10^{14}$  n/cm<sup>2</sup>/second (calculated at 175 MW of ETR power).

Table 7-17. Principal and trace elements in the beryllium reflector from the Materials Test Reactor. The same concentrations are assumed to apply to beryllium reflectors in the Engineering Test Reactor.

Element Symbol	Element Name	Number	Atomic Weight	Average KBI Beryllium Concentration (ppm by wt)	Estimated Inventory for a 2,000-kg MTR Beryllium Reflector Mass (g)	Actual Modeled ORIGEN2 Input Data Mass (g)	Ratio Estimated/ Modeled
H	Hydrogen	1	1.0079		0.000	0.000	
He	Helium	2	4.0026		0.000	0.000	
Li	Lithium	3	6.9410	1.000	2.000	2.000	1.000E+00
Be	Beryllium	4	9.0122	980,667.835	1,961,335.670	1,961,000.000	1.000E+00
B	Boron	5	10.8110	1.917	3.833	3.833	1.000E+00
C	Carbon	6	12.0110	745.000	1,490.000	1,490.000	1.000E+00
N	Nitrogen	7	14.0067	205.400	410.800	410.800	1.000E+00
O	Oxygen	8	15.9994	12,618.667	25,237.333	25,240.000	9.999E-01
F	Fluorine	9	18.9984	69.167	138.333	138.300	1.000E+00
Ne	Neon	10	20.1797	1,425.000	2,850.000	2,850.000	1.000E+00
Na	Sodium	11	22.9898	0.874	1.749	1.749	9.998E-01
Mg	Magnesium	12	24.3050	45.000	90.000	90.000	1.000E+00
Al	Aluminum	13	26.9815	355.833	711.667	711.700	1.000E+00
Si	Silicon	14	28.0855	364.167	728.333	728.300	1.000E+00
P	Phosphorus	15	30.9738	50.000	100.000	100.000	1.000E+00
S	Sulfur	16	32.0660	7.500	15.000	15.000	1.000E+00

Table 7-17. (continued).

Element Symbol	Element Name	Number	Atomic Weight	Average KBI Beryllium Concentration (ppm by wt)	Estimated Inventory for a 2,000-kg MTR Beryllium Reflector Mass (g)	Actual Modeled ORIGEN2 Input Data Mass (g)	Ratio Estimated/ Modeled
Cl	Chlorine	17	35.4527	50.000	100.000	100.000	1.000E+00
Ar	Argon	18	39.9480	6.370	12.740	12.740	1.000E+00
K	Potassium	19	39.0983	13.070	26.140	26.140	1.000E+00
Ca	Calcium	20	40.0780	200.000	400.000	400.000	1.000E+00
Sc	Scandium	21	44.9559	2.300	4.600	4.600	1.000E+00
Ti	Titanium	22	47.8800	61.667	123.333	123.300	1.000E+00
V	Vanadium	23	50.9415	3.423	6.847	6.847	1.000E+00
Cr	Chromium	24	51.9961	92.500	185.000	185.000	1.000E+00
Mn	Manganese	25	54.9381	56.667	113.333	113.300	1.000E+00
Fe	Iron	26	55.8470	1,499.167	2,998.333	2,998.000	1.000E+00
Co	Cobalt	27	58.9332	12.000	24.000	24.000	1.000E+00
Ni	Nickel	28	58.6900	225.833	451.667	451.700	9.999E-01
Cu	Copper	29	63.5460	87.500	175.000	175.000	1.000E+00
Zn	Zinc	30	65.3900	13.000	26.000	26.000	1.000E+00
Ga	Gallium	31	69.7230	0.859	1.719	1.719	9.998E-01
Ge	Germanium	32	72.6100	5.000	10.000	10.000	1.000E+00
As	Arsenic	33	74.9216	1.782	3.564	3.564	1.000E+00
Se	Selenium	34	78.9600	2.383	4.767	4.767	9.999E-01
Br	Bromine	35	79.9040	52.000	104.000	104.000	1.000E+00
Kr	Krypton	36	83.8000	85.167	170.333	170.300	1.000E+00
Rb	Rubidium	37	85.4678	7.767	15.533	15.530	1.000E+00
Sr	Strontium	38	87.6200	6.000	12.000	12.000	1.000E+00
Y	Yttrium	39	88.9059	1.000	2.000	2.000	1.000E+00
Zr	Zirconium	40	91.2240	38.214	76.429	76.430	1.000E+00
Nb	Niobium	41	92.9064	11.700	23.400	23.400	1.000E+00
Mo	Molybdenum	42	95.9400	10.000	20.000	20.000	1.000E+00
Tc	Technetium	43	98.9062		0.000	0.000	
Ru	Ruthenium	44	101.0700	5.000	10.000	10.000	1.000E+00
Rh	Rhodium	45	102.9055	0.994	1.987	1.987	1.000E+00
Pd	Palladium	46	106.4200	5.000	10.000	10.000	1.000E+00
Ag	Silver	47	107.8682	2.167	4.333	4.333	1.000E+00
Cd	Cadmium	48	112.4110	1.000	2.000	2.000	1.000E+00
In	Indium	49	114.8200	0.069	0.137	0.137	9.998E-01
Sn	Tin	50	118.7100	3.000	6.000	6.000	1.000E+00
Sb	Antimony	51	121.7500	0.241	0.481	0.481	9.999E-01
Te	Tellurium	52	127.6000	47.467	94.933	94.930	1.000E+00
I	Iodine	53	126.9045	10.000	20.000	20.000	1.000E+00
Xe	Xenon	54	131.2900	537.333	1,074.667	1,075.000	9.997E-01
Cs	Cesium	55	132.9054	0.201	0.403	0.403	9.999E-01
Ba	Barium	56	137.3270	6.000	12.000	12.000	1.000E+00
La	Lanthanum	57	138.9055	1.000	2.000	2.000	1.000E+00
Ce	Cerium	58	140.1150	1.000	2.000	2.000	1.000E+00
Pr	Praseodymium	59	140.9077	1.000	2.000	2.000	1.000E+00
Nd	Neodymium	60	144.2400	5.000	10.000	10.000	1.000E+00

Table 7-17. (continued).

Element Symbol	Element Name	Number	Atomic Weight	Average KBI Beryllium Concentration (ppm by wt)	Estimated Inventory for a 2,000-kg MTR Beryllium Reflector Mass (g)	Actual Modeled ORIGEN2 Input Data Mass (g)	Ratio Estimated/ Modeled
Pm	Promethium	61	144.9145		0.000	0.000	
Sm	Samarium	62	150.3600	0.500	1.000	1.000	1.000E+00
Eu	Europium	63	151.9650	0.500	1.000	1.000	1.000E+00
Gd	Gadolinium	64	157.2500	0.200	0.400	0.400	1.000E+00
Tb	Terbium	65	158.9253	1.000	2.000	2.000	1.000E+00
Dy	Dysprosium	66	162.5000	0.200	0.400	0.400	1.000E+00
Ho	Holmium	67	164.9303	1.000	2.000	2.000	1.000E+00
Er	Erbium	68	167.2600	0.500	1.000	1.000	1.000E+00
Tm	Thulium	69	168.9342	0.500	1.000	1.000	1.000E+00
Yb	Ytterbium	70	173.0400	0.200	0.400	0.400	1.000E+00
Lu	Lutetium	71	174.9670	0.667	1.333	1.333	1.000E+00
Hf	Hafnium	72	178.4900	0.423	0.847	0.847	1.000E+00
Ta	Tantalum	73	180.9479	0.433	0.866	0.866	1.000E+00
W	Tungsten	74	183.8500	76.214	152.428	152.400	1.000E+00
Re	Rhenium	75	186.2070	0.644	1.288	1.288	1.000E+00
Os	Osmium	76	190.2000	0.637	1.274	1.274	1.000E+00
Ir	Iridium	77	192.2200	0.005	0.010	0.010	1.000E+00
Pt	Platinum	78	195.0800	101.867	203.734	203.700	1.000E+00
Au	Gold	79	196.9665	24.800	49.600	49.600	1.000E+00
Hg	Mercury	80	200.5900	4.073	8.146	8.146	1.000E+00
Tl	Thallium	81	204.3833	25.000	50.000	50.000	1.000E+00
Pb	Lead	82	207.2000	1.000	2.000	2.000	1.000E+00
Bi	Bismuth	83	208.9804		0.000	0.000	
Po	Polonium	84			0.000	0.000	
At	Astatine	85			0.000	0.000	
Rn	Radon	86			0.000	0.000	
Fr	Francium	87			0.000	0.000	
Ra	Radium	88			0.000	0.000	
Ac	Actinium	89			0.000	0.000	
Th	Thorium	90	232.0381	0.438	0.876	0.876	1.000E+00
Pa	Protactinium	91			0.000	0.000	
U	Uranium	92	238.0289	30.000	60.000	60.000	1.000E+00
Np	Neptunium	93			0.000	0.000	
Pu	Plutonium	94			0.000	0.000	
Am	Americium	95			0.000	0.000	
Totals =				1,000,000.000	2,000,000.000	1,999,666.830	

KBI = Kawecki Berylco Industries

MTR = Materials Test Reactor

ORIGEN2 = Oak Ridge Isotope GENeration and Depletion Code Version 2

Table 7-18. Calculated inventory using Oak Ridge Isotope Generation and Depletion Code Version 2 for beryllium blocks from Core 1, Materials Test Reactor (irradiated from March 31, 1952, to July 1, 1969).

Isotope	Half-Life (years)	MTR Be Inventory on 07/01/69, End of Irradiation Date (Ci)	Materials Test Reactor Be Inventory on 04/21/70, Estimated Disposal Date (Ci)	Materials Test Reactor Be Inventory on 07/02/77, Estimated Disposal Date (Ci)	Materials Test Reactor Be Inventory on 09/15/01, Common Decay Date (Ci)
H-3	1.23E+01	1.45E+06	4.27E+05	6.45E+05	2.38E+05
Be-10	1.60E+06	3.64E+00	1.12E+00	2.52E+00	3.64E+00
C-14	5.73E+03	2.93E+01	9.01E+00	2.02E+01	2.91E+01
Cl-36	3.01E+05	3.47E-01	1.07E-01	2.40E-01	3.47E-01
Co-60	5.27E+00	2.82E+03	7.81E+02	6.94E+02	4.07E+01
Ni-59	7.60E+04	5.54E-01	1.71E-01	3.84E-01	5.54E-01
Ni-63	1.00E+02	1.05E+02	3.21E+01	6.85E+01	8.23E+01
Sr-90	2.91E+01	1.27E+01	3.82E+00	7.26E+00	5.88E+00
Nb-94	2.00E+04	7.74E-02	2.38E-02	5.35E-02	7.73E-02
Tc-99	2.13E+05	5.02E-03	1.55E-03	3.48E-03	5.02E-03
I-129	1.57E+07	3.94E-05	1.21E-05	2.73E-05	3.94E-05
Cs-137	3.02E+01	4.29E+01	1.30E+01	2.47E+01	2.04E+01
Eu-152	1.35E+01	3.47E-02	1.03E-02	1.61E-02	6.72E-03
Eu-154	8.59E+00	3.42E+01	9.86E+00	1.26E+01	2.55E+00
Pb-210	2.23E+01	3.61E-10	1.10E-10	2.07E-10	2.71E-10
Ra-226	1.60E+03	3.74E-11	1.30E-11	6.34E-11	4.03E-10
Ra-228	5.76E+00	6.90E-08	2.16E-08	5.28E-08	8.17E-08
Ac-227	2.18E+01	2.65E-07	9.07E-08	3.64E-07	1.02E-06
Th-228	1.91E+00	5.72E-04	1.94E-04	5.18E-04	6.03E-04
Th-229	7.30E+03	2.10E-07	6.97E-08	2.54E-07	8.51E-07
Th-230	7.54E+04	1.37E-08	4.35E-09	1.29E-08	4.30E-08
Th-232	1.40E+10	8.22E-08	2.53E-08	5.69E-08	8.22E-08
Pa-231	3.28E+04	1.45E-06	4.45E-07	1.00E-06	1.45E-06
U-232	7.00E+01	8.00E-04	2.45E-04	5.14E-04	5.87E-04
U-233	1.59E+05	2.04E-04	6.51E-05	1.46E-04	2.11E-04
U-234	2.46E+05	5.80E-05	1.81E-05	5.53E-05	1.41E-04
U-235	7.04E+08	7.72E-09	2.40E-09	5.75E-09	1.01E-08
U-236	2.34E+07	3.24E-06	9.99E-07	2.26E-06	3.36E-06

Table 7-18. (continued).

Isotope	Half-Life (years)	MTR Be Inventory on 07/01/69, End of Irradiation Date (Ci)	Materials Test Reactor Be Inventory on 04/21/70, Estimated Disposal Date (Ci)	Materials Test Reactor Be Inventory on 07/02/77, Estimated Disposal Date (Ci)	Materials Test Reactor Be Inventory on 09/15/01, Common Decay Date (Ci)
U-238	4.47E+09	1.41E-05	4.44E-06	9.97E-06	1.44E-05
Np-237	2.14E+06	7.36E-06	2.29E-06	5.69E-06	1.48E-05
Pu-238	8.77E+01	8.83E-01	3.02E-01	6.69E-01	7.98E-01
Pu-239	2.41E+04	7.57E-02	2.35E-02	5.27E-02	7.61E-02
Pu-240	6.56E+03	1.02E-01	3.19E-02	7.87E-02	1.33E-01
Pu-241	1.44E+01	3.62E+01	1.07E+01	1.72E+01	7.68E+00
Pu-242	3.75E+05	2.54E-03	7.81E-04	1.75E-03	2.54E-03
Pu-244	8.00E+07	1.72E-09	5.29E-10	1.19E-09	1.72E-09
Am-241	4.33E+02	1.28E-01	5.33E-02	3.48E-01	1.04E+00
Am-243	7.37E+03	3.13E-02	9.64E-03	2.17E-02	3.12E-02
Cm-243	2.91E+01	1.48E-02	4.46E-03	8.44E-03	6.75E-03
Cm-244	1.81E+01	1.60E+01	4.78E+00	8.20E+00	4.67E+00
Cm-245	8.50E+03	1.26E-03	3.89E-04	8.73E-04	1.26E-03
Cm-246	4.76E+03	1.69E-03	5.22E-04	1.17E-03	1.69E-03
Cm-247	1.56E+07	1.11E-0-8	3.42E-09	7.67E-09	1.11E-08
Cm-248	3.48E+05	8.56E-08	2.64E-08	5.95E-08	8.60E-08
Average transuranic concentration (nCi/g) =		620	694	854	1050.04
Beryllium mass (g) =		2,000,000	616,000	1,384,000	2,000,000
Metal volume (m <sup>3</sup> ) =		1.0811	0.333	0.748	1.0811
file=MTR3.wb1					
30.2% of Core 1 was disposed of on 4/21/70 and 69.8% disposed of on 7/02/77					

A total energy generation of 374,498 MWd over 4,520 days produces an average thermal reactor power of 84.07 MW, or an equivalent (steady-state) total neutron flux of  $2.368 \times 10^{14}$  n/cm<sup>2</sup>/second (e.g.,  $4.93 \times 10^{14} \times 84.07/175$ ) at ETR's beryllium reflector during the entire 4,520 days of operation for Core 1. The results of the ORIGEN2 calculation for selected radionuclides are listed in Table 7-19. Note that the calculated C-14 inventory for ETR's beryllium reflector at the time of disposal of this material in the SDA is 21.6 Ci. The calculated C-14 inventory for ETR also is shown in Table 1-1.

Table 7-19. Calculated inventory using Oak Ridge Isotope Generation and Depletion Code Version 2 for beryllium blocks from Core 1, Engineering Test Reactor (irradiated from October 15, 1957, to March 1, 1970).

Isotope	Half-Life (years)	ETR Be Inventory on 03/01/70, End of Irradiation Date (Ci)	ETR Be Inventory on 12/01/70, Estimated Disposal Date (Ci)	ETR Be Inventory on 09/15/01, Common Decay Date (Ci)
H-3	1.23E+01	1.22E+06	1.21E+06	2.08E+05
Be-10	1.60E+06	2.73E+00	2.73E+00	2.73E+00
C-14	5.73E+03	2.17E+01	2.17E+01	2.16E+01
Cl-36	3.01E+05	2.29E-01	2.29E-01	2.29E-01
Co-60	5.27E+00	2.04E+03	1.99E+03	3.21E+01
Ni-59	7.60E+04	2.34E-01	2.34E-01	2.3E-01
Ni-63	1.00E+02	6.51E+01	6.50E+01	5.13E+01
Sr-90	2.91E+01	8.47E+00	8.44E+00	4.00E+00
Nb-94	2.00E+04	4.824E-02	4.824E-02	4.82E-02
Tc-99	2.13E+05	2.47E-03	2.47E-03	2.41E-03
I-129	1.57E+07	2.50E-05	2.50E-05	2.50E-05
Cs-137	3.02E+01	3.01E+01	3.00E+01	1.45E+01
Eu-152	1.35E+01	1.40E-03	1.39E-03	2.81E-04
Eu-154	8.59E+00	5.23E+00	5.15E+00	4.11E-01
Pb-210	2.23E+01	6.24E-10	6.27E-10	2.804E-10
Ra-226	1.60E+03	1.06E-11	1.11E-11	1.25E-10
Ra-228	5.76E+00	1.52E-08	1.53E-08	2.04E-08
Ac-227	2.18E+01	3.41E-08	3.60E-08	2.64E-07
Th-228	1.91E+00	2.29E-04	2.39E-04	3.09E-04
Th-229	7.30E+03	5.56E-08	5.64E-08	2.18E-07
Th-230	7.54E+04	5.42E-09	5.44E-09	1.18E-08
Th-232	1.40E+10	2.06E-08	2.06E-08	2.06E-08
Pa-231	3.28E+04	3.97E-07	3.97E-07	3.97E-07
U-232	7.00E+01	4.07E-04	4.07E-04	3.01E-04
U-233	1.59E+05	4.90E-05	5.35E-05	5.47E-05
U-234	2.46E+05	1.81E-05	1.82E-05	2.68E-05
U-235	7.04E+08	1.64E-09	1.64E-09	2.11E-09
U-236	2.34E+07	6.06E-07	6.06E-07	6.48E-07
U-238	4.47E+09	2.83E-06	2.83E-06	2.83E-06
Np-237	2.14E+06	1.61E-06	1.63E-06	2.94E-06
Pu-238	8.77E+01	7.91E-02	8.59E-02	8.53E-02
Pu-239	2.41E+04	1.47E-02	1.50E-02	1.50E-02
Pu-240	6.56E+03	2.05E-02	2.09E-02	6.02E-02
Pu-241	1.44E+01	7.60E+00	7.54E+00	1.67E+00
Pu-242	3.75E+05	8.64E-04	8.64E-04	8.65E-04



Table 7-19. (continued).

Isotope	Half-Life (years)	ETR Be Inventory on 03/01/70, End of Irradiation Date (Ci)	ETR Be Inventory on 12/01/70, Estimated Disposal Date (Ci)	ETR Be Inventory on 09/15/01, Common Decay Date (Ci)
Pu-244	8.00E+07	5.14E-09	5.14E-09	5.14E-09
Am-241	4.33E+02	8.12E-03	1.01E-02	2.00E-01
Am-243	7.37E+03	1.35E-02	1.35E-02	1.35E-02
Cm-243	2.91E+01	3.27E-03	3.26E-03	1.52E-03
Cm-244	1.81E+01	2.05E+01	2.04E+01	6.13E+00
Cm-245	8.50E+03	1.81E-03	1.81E-03	1.80E-03
Cm-246	4.76E+03	9.00E-03	9.00E-03	8.96E-03
Cm-247	1.56E+07	1.15E-07	1.15E-07	1.15E-07
Cm-248	3.48E+05	2.85E-06	2.86E-06	2.94E-06
Average transuranic concentration (nCi/g) =		242	257	62
Beryllium mass (g) =		624,000	624,000	624,000
Metal volume (m <sup>3</sup> ) =		0.3373	0.3373	0.3373
ETR = Engineering Test Reactor				

